130 ENVIRONMENTAL PARK

APPENDIX IIIA2 SURFACE WATER DRAINAGE CALCULATIONS



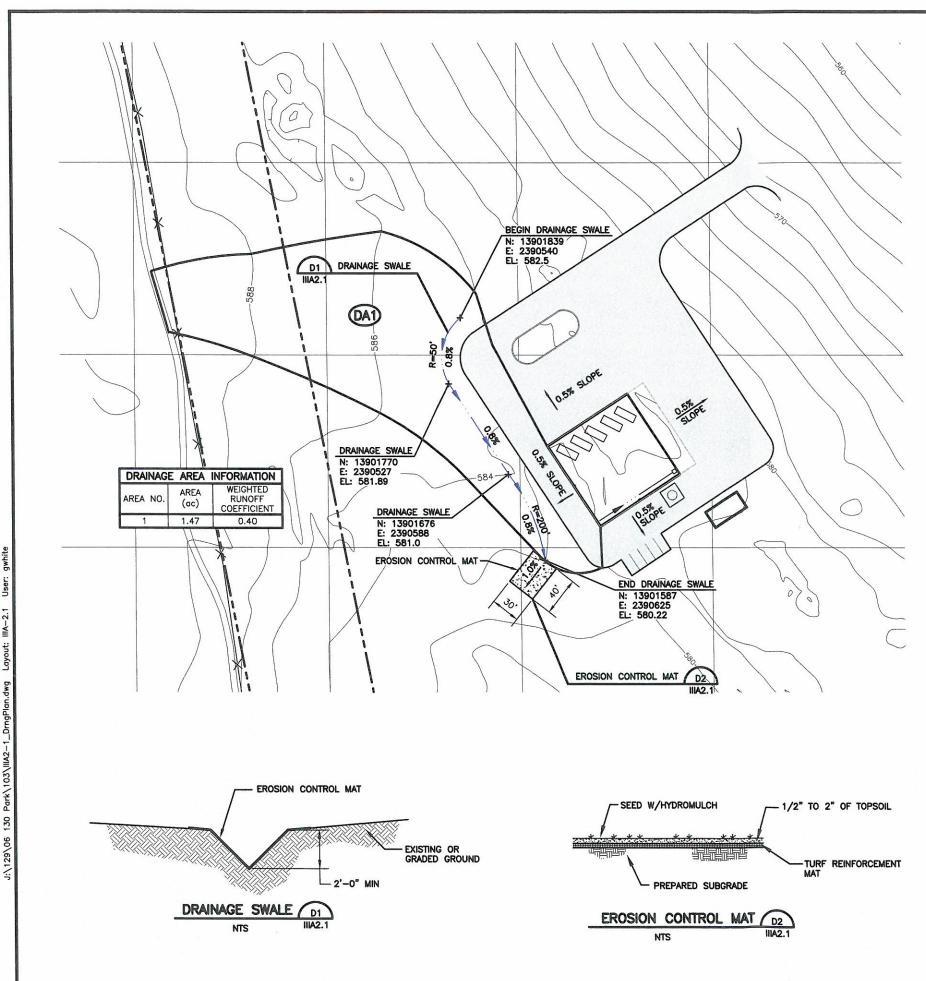
Biggs & Mathews Environmental, Inc. Firm Registration No. F-256

7/11/14

Includes pages IIIA2-1 th rough IIIA2-4

SURFACE WATER DRAINAGE CALCULATIONS

The drainage swale design calculations are depicted for the surface water management system to manage run-on from the contributing drainage area by directing surface water around the transfer station facility and to manage uncontaminated surface water runoff from the transfer station. The procedures in the Texas Department of Transportation (TXDOT), Hydraulic Design Manual, October 2011 were used to determine the 25-year peak flow rate, normal flow depth and capacity, and velocity for the design of the swale.





LEGEND PROPERTY BOUNDARY --- FACILITY BOUNDARY 560 EXISTING CONTOUR - DRAINAGE AREA

NOTE:

1. CONTOURS AND ELEVATIONS PROVIDED BY DALLAS AERIAL SERVICE FROM AERIAL PHOTOGRAPHY FLOWN MAY 13, 2013. HORIZONTAL DATUM IS TEXAS STATE PLANE COORDINATE SYSTEM, SOUTH CENTRAL ZONE (NAD 83). ELEVATIONS ARE RELATIVE TO NAVD88 — GEOID 12A.



DRAINAGE DESIGN PLAN

130 ENVIRONMENTAL PARK, LLC 130 ENVIRONMENTAL PARK TYPE V REGISTRATION APPLICATION



BIGGS & MATHEWS ENVIRONMENTAL

MANSFIELD + WICHITA FALLS

IS	SUED	FOR REGISTRATIO	N PUR	POS	ES O	NLY		Westri	ng Body	NSFIELD • WICHITA 817-563-1144	
		. REVISIONS					Т	BPE FIRM	NO. F-256	TBPG FIRM I	10. 50222
							DSN.	CRH	DATE : 07/14		DRAWING
							DWN.	SRC	SCALE : GRAPH	IIC	HIAO
REV	DATE	DESCRIPTION	DWN BY	DES BY	CHK BY	APP BY	снк.	JHP	DWG : IIIA2-1_	DrngPlan.dwg	IIIA2.

130 Environmental Park Transfer Station Registration Drainage Swale Calculations

Required: Calculate the design flow rate, normal depth, and velocity in the drainage swale.

Methods:

- 1. Calculate the 25-year peak flow rate (Q) for the drainage area using the Rational Method.
- 2. Calculate the normal depth and velocity for the draingage swale discharge by applying Manning's Equation.

References:

- 1. United States Geologic Survey, Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas, 2004.
- 2. Texas Department of Transportation, Hydraulic Design Manual, Revised October 2011.
- 3. Strum, Terry W., Open Channel Hydraulics, 2nd. Edition, 2010

Solution:

1. Calculate the 25-year peak flow rate (Q) for the drainage area using the Rational Method.

```
25-Year Rainfall Depth (Pd) =
                               1.52 in
                                            (ref 1, extrapolated for 10 minutes)
  Time of Concentration (tc) =
                                  10 min
                                            (conservative minimum value)
         Rainfall Intensity (I) =
                                  9.1 in/hr (ref 2, I = Pd/tc)
      Runoff Coefficient (C) =
                               0.40
                                            (ref 2, Table 4-10)
                   Area (A) = 1.47 acre
25-Year Peak Flow Rate (Q) =
                                 CIA cfs
                         Q = (0.4)(9.1)(1.47)
                         Q = 5.4 cfs
```

2. Use Manning's equation to calculate the normal depth in the diversion swale for the drainage area.

List of Symbols:

Q = design flow rate for channel, cfs

R = hydraulic radius, ft

n = Manning's roughness coefficient

S = channel slope, ft/ft

m = ratio of run to rise for channel sideslope

A_o = flow area, sf

 $g = gravitational acceleration = 32.2 ft/s^2$

B = top width of flow, ft

y = normal flow depth of diversion channel, ft

Design Inputs:

Q = 5.4 cfs

S = 0.008 ft/ft

m = 5 (H): 1 (V)

n = 0.022 (ref 3, Table 4.1, Typical value for excavated channel)

130 Environmental Park Transfer Station Registration Drainage Swale Calculations

Step 1 - Based on the geometry of the swale cross-section, solve for R and $A_{\scriptscriptstyle 0}$:

R =
$$\frac{A_0}{2y(1+m^2)^{0.5}}$$
 (ref 3, Table 2.1)
 $A_0 = my^2$ (ref 3, Table 2.1)

Solve Manning's equation for flow depth (y) based on previously calculated Q_0 .

$$Q_o = \frac{1.49}{n} A_o R^{2/3} S^{1/2}$$
y = 0.63 ft
$$R = 0.308 \text{ ft}$$

$$A_o = 1.97 \text{ sf}$$

Step 2 - Solve for velocity in the diversion swale.

$$Q = VA \Longrightarrow$$
 $V = Q/A$ $V = 2.72 \text{ ft/s}$

130 Environmental Park Transfer Station Registration Drainage Calculations at Discharge

Required: Calculate the design flow rate, normal depth, and velocity at the discharge for the drainage swale.

Methods:

- 1. Calculate the 25-year peak flow rate (Q) for the drainage area using the Rational Method.
- 2. Calculate the normal depth and velocity for the draingage swale by applying Manning's Equation.

References:

- 1. United States Geologic Survey, Atlas of Depth-Duration Frequency of Precipitation Annual Maxima for Texas, 2004.
- 2. Texas Department of Transportation, Hydraulic Design Manual, Revised October 2011.
- 3. Strum, Terry W., Open Channel Hydraulics, 2nd. Edition, 2010

Solution:

1. Calculate the 25-year peak flow rate (Q) for the drainage area using the Rational Method.

25-Year Rainfall Depth (Pd) = 1.52 in (ref 1, extrapolated for 10 minutes) Time of Concentration (tc) = 10 min (conservative minimum value) Rainfall Intensity (I) = 9.1 in/hr (ref 2, I = Pd/tc) (ref 2, Table 4-10) Area (A) = 1.47 acre 25-Year Peak Flow Rate (Q) = CIA cfs
$$Q = (0.4)(9.1)(1.47)$$
$$Q = 5.4 cfs$$

2. Use Manning's equation to calculate the normal depth and velocity at the erosion mat discharge.

List of Symbols:

Q_o = design flow rate at discharge, cfs

S = erosion control mat slope, ft/ft

n = Manning's roughness coefficient

B = top width of flow, ft

A_o = flow area, sf

y = normal flow depth of diversion channel, ft

Design Inputs:

$$Q_o = 5.4$$
 cfs

$$S = 0.01$$
 ft/ft

$$B = 30 f$$

n = 0.03 (ref 3, Table 4.1, Typical value for vegetal channel)

Calculations:

$$y = \left[\frac{(Q_o \times n)}{1.486 \times B \times S^{1/2}} \right]^{0.6}$$

$$y = 0.136 \text{ ft.}$$

$$A_o = y \times B$$

 $A_o = 4.088 \text{ sf}$

$$v = \frac{Q_o}{A_o}$$

$$v = 1.312 \text{ fps}$$

Summary: The runoff velocity leaving the erosion control mat at the discharge is less than 5 fps.

130 ENVIRONMENTAL PARK CALDWELL COUNTY, TEXAS TCEQ REGISTRATION NO. MSW 40269

TYPE V REGISTRATION APPLICATION

PART III FACILITY INVESTIGATION AND DESIGN

APPENDIX IIIC CLOSURE PLAN

Prepared for

130 ENVIRONMENTAL PARK, LLC

August 2013 Revised February 2014

Revised July 2014

J. HEATH PARKER
94764
CENSE
SIONAL
Biggs & Mathews Environmental, Inc.
Firm Registration No. F-256

Prepared by

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TEXAS BOARD OF PROFESSIONAL ENGINEERS FIRM REGISTRATION No. F-256

TEXAS BOARD OF PROFESSIONAL GEOSCIENTISTS FIRM REGISTRATION NO. 50222

And

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2500 Brook Avenue • Wichita Falls, Texas 76301 • 940-766-0156

Texas Board of Professional Engineers
Firm Registration No. F-834

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30 TAC §330.459

At the time of closure, 130 Environmental Park <u>Transfer Station</u> will remove all waste, waste residues, and any recovered materials. The transfer station units shall either be dismantled and removed off-site or decontaminated. All material on-site, whether in process or processed will be evacuated to an authorized facility and the tipping floors, processing areas, and post-processing areas will be disinfected. A layout of the transfer station facility is provided in Appendix IIIB as Drawing IIIB.1.

No later than 90 days prior to the initiation of final closure, 130 Environmental Park Transfer Station shall, through a public notice in the newspaper(s) of largest circulation in the vicinity of the facility, provide public notice for final facility closure. This notice will include the name, address, and physical location of the facility, the registration number, and the last day of intended receipt of materials for processing at the facility. 130 Environmental Park Transfer Station will also make available an adequate number of copies of the approved Closure Plan for public review. The owner/operator will also provide written notification to the TCEQ of the intent to close the facility and place this Notice of Intent in the site operating record.

Initiation of closure activities for the facility will begin after the date on which the facility receives the known final receipt of waste to be processed.

The following steps will be taken:

- Notify the TCEQ.
- No later than 90 days prior to the initiation of final closure, post a minimum of one sign at the main entrance and all other frequently used points of access for the facility notifying all persons who may utilize the facility of the date of closing for the facility and the prohibition against further receipt of waste materials after the stated date.
- No later than 90 days prior to the initiation of final closure, install suitable barriers
 to all gates or access points or alternatively, fence around the entire waste
 processing area, to adequately prevent the unauthorized dumping of solid waste
 at the closed facility.
- Remove wastes, waste residues, and any recovered materials for disposal at an appropriate off-site location.
- Dismantle and remove or decontaminate facility units.
- Wash transfer station tipping floor and any surfaces that have been in contact with waste.
- Disinfect the tipping floor, processing area, and post-processing areas.
- Perform facility inspection and prepare certification of closure.
- If there is evidence of a release from the transfer station, the executive director may require an investigation into the nature and extent of the release and an assessment of measures necessary to correct an impact to groundwater.

3 CERTIFICATION OF FINAL FACILITY CLOSURE

30 TAC §330.461

Following completion of all final closure activities for the transfer station, 130 Environmental Park <u>Transfer Station</u> will submit within 10 days to the executive director for review and approval a documented certification signed by an independent registered professional engineer, verifying that final closure has been completed in accordance with the approved Closure Plan and the applicable rule provisions of 30 TAC Chapter 330 Subchapter K. The submittal to the executive director shall include all applicable documentation necessary for certification of final closure.

Within 10 days after completion of final closure activities for the facility, 130 Environmental Park <u>Transfer Station</u> will submit to the executive director a request for voluntary revocation of the facility's registration.

Following receipt of the required final closure documents, as applicable, the commission's regional office will conduct an inspection and provide a report verifying proper closure of the facility according to the approved Closure Plan before termination of operation and closure of the facility will be acknowledged and the facility deemed properly closed.

The provisions of §330.461(c)(1) and (d) do not apply to the transfer station as no wastes will remain at the closed facility.

130 ENVIRONMENTAL PARK CALDWELL COUNTY, TEXAS TCEQ REGISTRATION NO. MSW 40269

TYPE V REGISTRATION APPLICATION

PART III FACILITY INVESTIGATION AND DESIGN

APPENDIX IIID COST ESTIMATE FOR CLOSURE

Prepared for

130 ENVIRONMENTAL PARK, LLC

August 2013 Revised February 2014

Revised July 2014



Prepared by

BIGGS & MATHEWS ENVIRONMENTAL

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TEXAS BOARD OF PROFESSIONAL ENGINEERS
FIRM REGISTRATION NO. F-834

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APPENDIX IIID1

Closure Cost Estimate Calculations 30 TAC §330.505

APPENDIX IIID2

Evidence of Financial Assurance 30 TAC §37.8031



APPENDIX IIID2 EVIDENCE OF FINANCIAL ASSURANCE 30 TAC §37.8031

Mr. Richard A. Hyde, P.E. Interim Executive Director Texas Commission on Environmental Quality P.O. Box 13087 Austin, Texas 78711-3087

Re:

130 Environmental Park Caldwell County, Texas

TCEQ Registration Application No. MSW 40269

Dear Mr. Hyde:

This letter is to provide Evidence of Financial Responsibility pursuant to 30 TAC §330.505(b) of the Municipal Solid Waste Management Regulations with respect to the above-referenced project.

130 Environmental Park, LLC agrees to provide financial assurance for this registration in accordance with the financial assurance schedule developed in Part III, Appendix IIID – Cost Estimate for Closure, or other amount specified by the Texas Commission on Environmental Quality (TCEQ).

In accordance with $\S 37.8031$ the assurance will be provided by, but is not limited to, one or more of the following:

- 1. Trust Fund
- 2. Surety Bond Guaranteeing Payment or Performance
- 3. Letter of Credit
- 4. Insurance
- 5. Corporate Guarantee

After this registration application is approved by TCEQ, 130 Environmental Park, LLC will file the required financial assurance. A copy of the documentation required to demonstrate financial assurance, as specified in 30 TAC Chapter 37, Subchapter R, will be submitted to the executive director of the TCEQ 60 days prior to the initial receipt of waste. The financial assurance will indicate the TCEQ as beneficiary and shall remain in full force and effect throughout the life of the registration.

ATTEST:

130 Environmental Park, LLC

Ernest Kaufmann

President and Manager

130 Environmental Park, LLC

130 ENVIRONMENTAL PARK CALDWELL COUNTY, TEXAS TCEQ REGISTRATION NO. MSW 40269

TYPE V REGISTRATION APPLICATION

PART III FACILITY INVESTIGATION AND DESIGN

APPENDIX IIIE COPY OF ATTACHMENT C2 – FLOOD CONTROL ANALYSIS FROM THE TYPE I (MSW 2383) PERMIT APPLICATION

Prepared for

130 ENVIRONMENTAL PARK, LLC

August 2013 Revised February 2014

Revised July 2014

Prepared by

BIGGS & MATHEWS ENVIRONMENTAL

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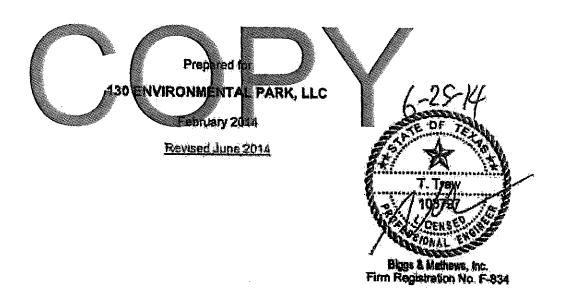
TEXAS BOARD OF PROFESSIONAL ENGINEERS
FIRM REGISTRATION No. F-834

130 ENVIRONMENTAL PARK CALDWELL COUNTY, TEXAS TCEQ PERMIT APPLICATION NO. MSW 2383

TYPE I PERMIT APPLICATION

PART III - FACILITY INVESTIGATION AND DESIGN

ATTACHMENT C2 FLOOD CONTROL ANALYSIS



Prepared by

BIGGS & MATHEWS ENVIRONMENTAL 1700 Robert Road, Suite 100 • Mansfield, Texas 76063 • 817-563-1144

TEXAS BOARD OF PROFESSIONAL ENGINEERS FIRM REGISTRATION NO. F-256 TEXAS BOARD OF PROFESSIONAL GEOSCIENTISTS FIRM REGISTRATION NO. 50222

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> Texas Board of Professional Engineers Firm Registration No. F-834

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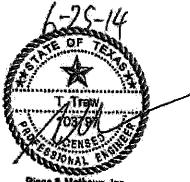
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Appendix C2-A Floodplain Maps

Appendix C2-B
Existing Condition HEC-HMS Evaluation

Appendix C2-C Existing Condition HEC-RAS Evaluation

Appendix C2-D
Postdevelopment Condition HEC-RAS Evaluation



Biggs & Mathews, Inc. Firm Registration No. F-834

1.1 Purpose

1

The flood control and analysis report is prepared as part of a permit application for 130 Environmental Park and includes the demonstrations consistent with the requirements of §§330.63(c)(2), 330.307, and 330.547. The flood control and analysis report demonstrates that solid waste disposal operations will not be located within the 100-year floodway as defined by the Federal Emergency Management Administration (FEMA), restrict the flow of the 100-year flood, reduce the temporary water storage capacity of the floodplain, or result in washout of solid waste so as to pose a hazard to human health and the environment.

130 Environmental Park is located in the San Marcos River drainage basin. Dry Creek traverses the property in a northeast to southwest direction and an unnamed tributary to Dry Creek traverses the property in a northwest to southeast direction. Both Dry Creek and the unnamed tributary enter the Soil Conservation Service (SCS) Site 21 Reservoir, located on Dry Creek within the 130 Environmental Park property. Dry Creek exits the SCS Site 21 Reservoir and enters Plum Creek approximately five miles south of the property. Plum Creek flows generally in a northwest to southeast direction, and enters the San Marcos River about 23 miles downstream from the property.

The flood control and analysis report is arganized to include a narrative description of the existing and postdeveloped conditions and a discussion of the various demonstrations. Drainage calculations are included in the appendices. Drainage design plans and details are included in Attachment C3. The following is a brief description of each of the appendices.

Appendix C2-A - Floodplain Maps

Appendix C2-A includes drawings demonstrating that no waste disposal operations shall be permitted in areas that are located in a 100-year floodway as defined by the Federal Emergency Management Agency (FEMA) and that the municipal solid waste storage and processing facilities shall be located outside of the 100-year floodplain. Appendix C2-A also includes drawings demonstrating that development of the 130 Environmental Park will not restrict the flow of the 100-year flood, will not reduce the temporary water storage capacity of the floodplain, and will not adversely impact Dry Creek, its unnamed tributary, or the SCS Site 21 Reservoir.

FEMA has defined the limits of the 100-year floodplain in the vicinity of the landfill as Zone A; no base flood elevations have been determined by FEMA. The limits of the floodplain are depicted on Drawing C2-A-1 - Flood Insurance Rate Map (FIRM), which is the drawing compiled from the FIRM Community Panel Number 48055C0125E, with an effective date of June 19, 2012. Drawing C2-A-1 includes the facility boundary, landfill footprint, and the limits of landfill grading depicted along with the limit of the FEMA

100-year floodplain. This drawing demonstrates that the proposed waste disposal units will not be located within the limits of the 100-year floodplain, based on the FEMA defined Zone A limits.

Drawing C2-A-2 – Existing Conditions Drainage Areas depicts the drainage areas contributing to Dry Creek, its unnamed tributary, and the SCS Site 21 Reservoir. A table is included with the area for each of the delineated areas. The facility and property boundary limits are also shown.

Drawing C2-A-3 – Existing Conditions Workmap depicts the delineation of the 100-year floodplain limits based upon the existing conditions. The facility and property boundary limits, and HEC-RAS cross section locations are shown. The limits of the FEMA Zone A are also depicted for information.

Drawing C2-A-4 – Postdeveloped Floodplain Workmap depicts the delineation of the 100-year floodplain limits based upon the existing conditions. The landfill footprint, limits of landfill grading, entrance road, and storage and processing facility locations are shown along with the facility and property boundary limits, and HEC-RAS cross section locations. The limits of the FEMA Zone A are also depicted for information.

Drawing C2-A-5 — Postdeveloped Floodplain Workmap Detail depicts the delineation of the 100-year floodplain limits based upon the existing conditions. This map depicts the landfill final completion plan and is produced at a scale to provide more detail comparing the limits of the 100-year floodplain with the landfill development. The landfill footprint, limits of landfill grading, entrance road, and storage and processing facility locations are shown along with the facility and property boundary limits, and HEC-RAS cross section locations. The limits of the FEMA Zone A are also depicted for information.

Appendix C2-B - Existing Condition HEC-HMS Evaluation

The existing condition HEC-HMS results for the floodplain evaluation are included in Appendix C2-B. The existing condition analysis includes delineation of drainage areas contributing to Dry Creek, its unnamed tributary, and the SCS Site 21 Reservoir. The results of the existing condition HEC-HMS evaluation are provided in the existing conditions summary, which provides results for the 25-year and 100-year events.

Appendix C2-C - Existing Condition HEC-RAS Evaluation

The existing condition HEC-RAS results are included in Appendix C2-C and represent the existing conditions. A summary table shows the results of the hydraulic analysis. The water surface elevation and energy grade line are graphically shown for each cross section.

Appendix C2-D - Postdeveloped Condition HEC-RAS Evaluation

The postdeveloped condition HEC-RAS results are included in Appendix C2-D and represent the postdeveloped conditions. A summary table shows the results of the hydraulic analysis. The water surface elevation and energy grade line are graphically shown for each cross section.

2 METHODOLOGY

2.1 Concepts and Methods

The hydrologic and hydraulic methods employed in this study are consistent with the TCEQ regulations. The United States Corps of Engineers (COE) HEC-HMS and HEC-RAS computer programs were used in the hydrologic and hydraulic analysis, respectively.

- Maps were prepared that provided information about the surface water runoff characteristics based on the existing conditions. These maps are included in Appendix C2-A.
- Surface water runoff hydrographs for the existing condition were developed in HEC-HMS. The HEC-HMS evaluation for the existing condition is in Appendix C2-B.
- Hydraulic models for the existing condition were developed to evaluate water surface elevations for Dry Creek, its unnamed tributary, and the SCS Site 21 Reservoir, under peak flow conditions using HEC-RAS is in Appendix C2-C.
- Hydraulic models for the postde eloped condition were developed to evaluate water surface elevations for Dr. Creek, its unnamed troutary, and the SCS Site 21 Reservoir under peak few conditions using HEC RAS is in Appendix C2-D.

3

3.1 HEC-HMS

The COE HEC-HMS program was developed to simulate the surface water runoff response of a watershed. The HEC-HMS model represents a watershed as a network of hydrologic and hydraulic components such as: sub-basins, reaches, reservoirs, junctions, and outlets. Specifically, HEC-HMS v3.5 was used to perform all of the hydrologic modeling. The following assumptions were made as part of the hydrologic modeling process:

- Precipitation: The meteorological model used was the frequency storm method
 which assumes precipitation rates that are temporally varied in 15 minute
 increments, but remain spatially unvaried across the entire watershed. This
 method uses the alternating block method of hyetograph distribution with the
 highest rainfall intensity occurring midway (50 percent) through the storm. A
 storm duration of 10 days was used in the model because it yielded the highest
 water surface elevation in the Site 21 reservoir and the largest peak discharges.
- Watershed Characteristics: The watershed characteristics considered in the analysis consist of rainfall loss, transform, and routing. Urban Hydrology for Small Watersheds, TR.55, describes the methods used for both rainfall loss and transform. Specifically, he (Soil Conservation Service) SCS runoff curve number method was used to analyze rainfall loss, while the SCS unit hydrograph method was used for transform. The routing method used in the analysis was the Kinematic Wave method.

3.2 Hydrologic Elements Naming Convention

The following naming convention was used in the existing hydrologic evaluations:

- UNT-1 drainage area contributing to the Unnamed Tributary west of the proposed landfill
- DC-1 drainage area contributing to Dry Creek on the east side of the proposed landfill

3.2.1 HEC-RAS

The COE HEC-RAS program was developed to evaluate gradually varied open channel flow in natural and man-made streams, as well as, the hydraulics related to structures such as bridges, culverts, dams, levees, etc. In this situation, separate models were created for both Dry Creek and the Unnamed Tributary network with both models using

the same downstream boundary condition resulting from the maximum water surface elevation in the Site 21 reservoir of 518.9 ft. Both streams were modeled in steady state and, as a result, the peak discharge applied does not change with time. The cross-sections for both models were taken from a combination of data listed in order of priority: on the ground survey delineating waters of the US, contours developed from aerial photography flown May 13, 2013, and contours available from CAPCOG. Manning's roughness coefficients for the channels and floodplain were determined through on-site investigation and aerial photos.

3.2.2 Hydraulic Elements Naming Convention

The following naming convention was used in the existing and post-developed hydraulic evaluations:

- A1.93 cross-section on Dry Creek at river station 1.93
- B0.59 cross-section on Unnamed Tributary at river station 0.59
- C0.41 cross-section on Tributary A at river station 0.41
- D0.53 cross-section on Tributary B at river station 0.53

The existing conditions modeling reflects the peak discharges and maximum water surface elevations in the Site 21 reservoir as identified from the hydrologic model.

The hydraulic model for existing conditions uses the existing topographic data with one culvert located on Dry Creek at the Hommanville Trail crossing. Both the 25 and 100 year events significantly overtop, by as much as 7 feet, the limited capacity of the 2 - 5 foot diameter corrugated metal pipes under Hommanville Trail.



The postdeveloped conditions modeling reflect the same lower peak discharges then that were identified in the existing conditions hydrologic model. The peak discharges in the condition are less than those in the existing condition as identified in Part III Attachment C1 of this application.

The changes to the postdeveloped conditions <u>hydraulic</u> model are limited to changes to the channel and floodplain geometry immediately upstream and downstream of where the proposed entrance road crosses the Unnamed Tributary and Tributary B. At the Unnamed Tributary crossing, 7 box culverts (7'H x 12'W) carry both the 100 and 25 year events without overtopping the entrance road. At the Tributary A-B crossing, a-two box culverts (4'H x 8'W) carryies both the 100 and 25 year events without overtopping the road, while the 100 year event overtops. In both locations, the culverts result in slight increases in the upstream water surface elevations. However, these increases terminate within the property boundary at cross-sections B8.74 and D2.4872. A comparison of existing/postdeveloped water surface elevations at each cross-section upstream of the culverts is shown in Tables 1 and 2.

130 Environmental Park
Table 1 - Upgamed Tributary Evisting/Postdeveloped Cross-section Comparison

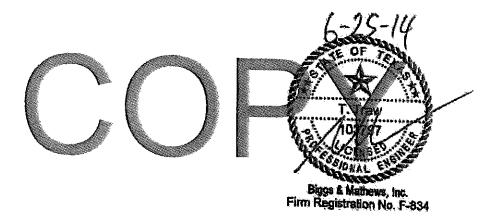
X-sec	River	25-Year Veter urface Elevation (ely lon (100 ear Wer So ace Elevation (ft.)			
Label	Station	Existing	<u>Post-</u> ∨eloped	Orference	– Existing	<u>vst-</u>	Difference	
B12	12	558.52/	8.52	0.01	559.03	59.02	-0.01	
B10.1	10.1	S-50	88.	0.0	550.74	50.74	0.00	
B9.73	9.73	548.18	548.18	0.00	548.64	548.63	7 7 7 7 2 10 10 10 10 10 10 10 10 10 10 10 10 10	
B9.12	9.12	545.68	545,68	00.0	546.15	546.16	- <u>D.01</u>	
88.74	8.74	544.46	544.46	0.00	545.06	The second secon	0.00	
B8.19	8.19	543,20	543.22	0.02	543.85	545,07 543,91	0.01	
B7B	7.9	542.57	542.62	0.05	543.21	543.32	0.06	
B7.56	7.56	541.24	541.48	0.24	541,97	THE RESERVE THE PARTY OF THE PA	0.11	
B7.26	7,26	540_15	540.28	0.18	540.99	542,37 541,28	0.40 0.29	

130 Environmental Park
Table 2 - Tributary B Existing/Postdeveloped Cross-section Comparis

X-sec	River	25-Year W	ster Surface El	evation (ft.)	Cross-section Comparison 100-Year Water Surface Elevation (ft.)		
Label	Station	Existing	Post- developed	Difference	Existing	Post- developed	Difference
D3,88	3,88	581. 3 0	581.30	0.00	581,50	581,50	0.00
D3.16	3.16	568.43	568.43	0.00	568.68	568.68	
D2.09	2.99	585.14	585.14	0.00	565,43	565.43	0.00
D2.9	2.9	563.55	563.55	0.00	563.82	The second secon	0.00
D2.72	2.72	557.32	557.32	0.00		563.82	0.00
D2.65	2,65	556.21	556.20	-0.01	557.72	557.72	0,00
D2.48	2.48	653,39	553,42	The same of the sa	556.58	556,58	0.00
D2.36	2.36	551.52	A STATE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN THE PERSON NAMED IN THE PERSON NAMED IN	0.03	553.70	\$53.70	0.00
D2.29	2.29	THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COL	551,46	-0.04	551.79	551.79	0.00
	2.27	549.62	550.43	0.81	549.93	551.32	1.39

In accordance with §330.547(a), 130 Environmental Park's waste disposal operations are not located in the 100-year floodway. In accordance with §330.547(b), 130 Environmental Park's new municipal solid waste disposal units are not located in the 100-year floodplain, will not restrict the flow of the 100-year flood, will not reduce the temporary water storage capacity of the floodplain, and will not result in the washout of solid waste. Further, in accordance with §330.547(c), 130 Environmental Park's processing and/or storage units are not located within the 100-year floodplain.

130 ENVIRONMENTAL PARK ATTACHMENT C2 APPENDIX C2-A FLOODPLAIN MAPS

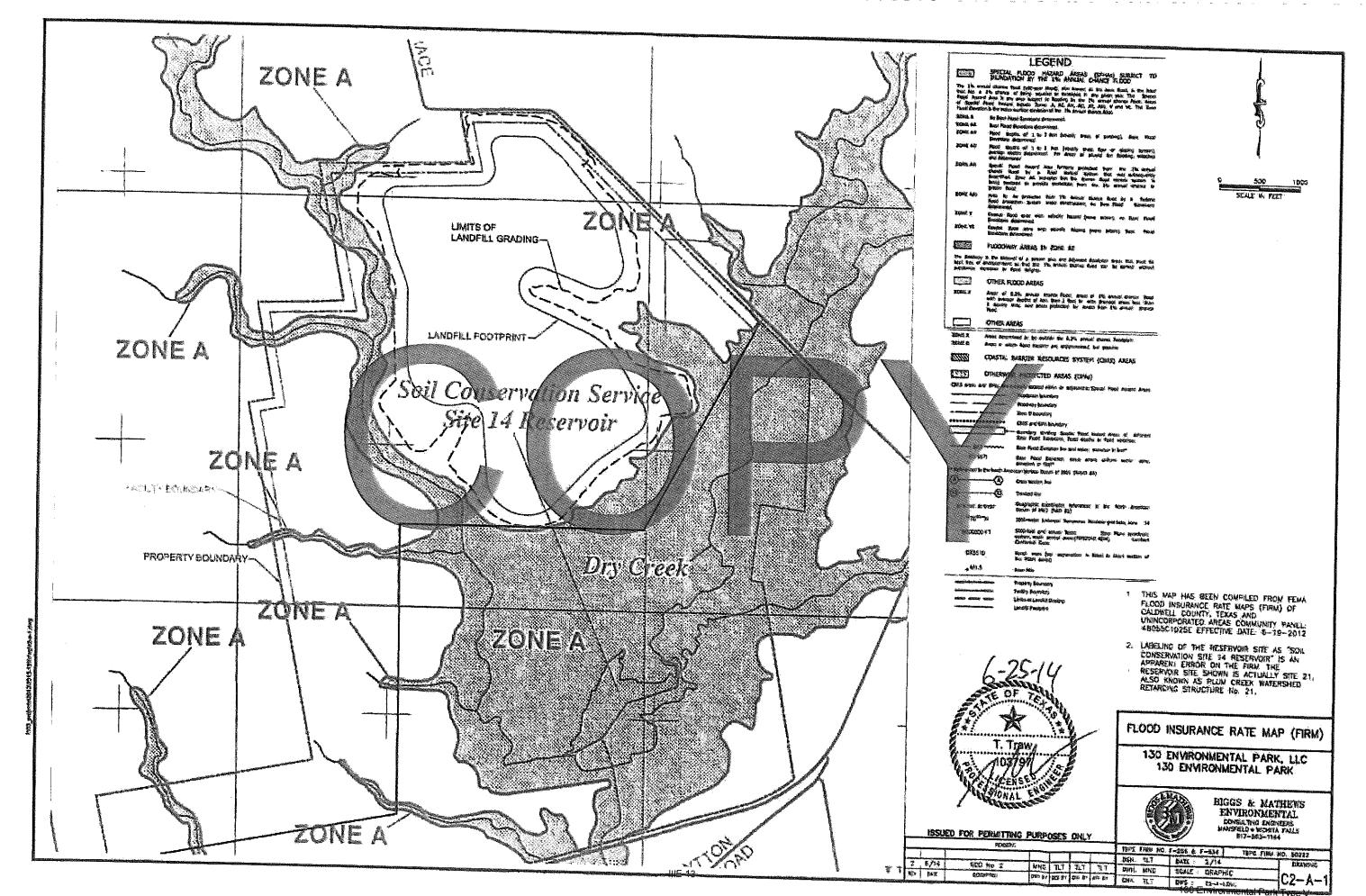


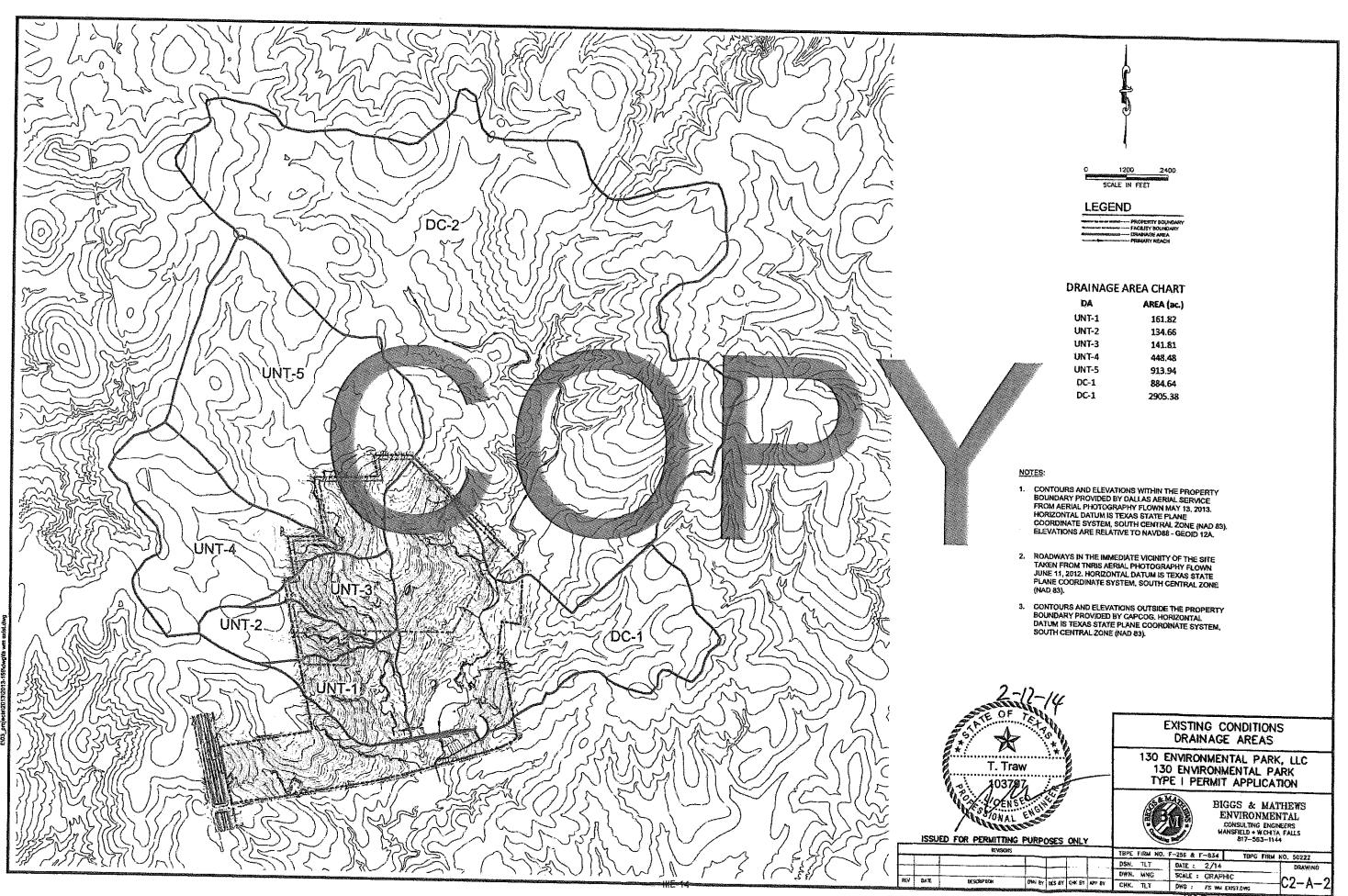
Includes pages C2-A-1 through C2-A-5

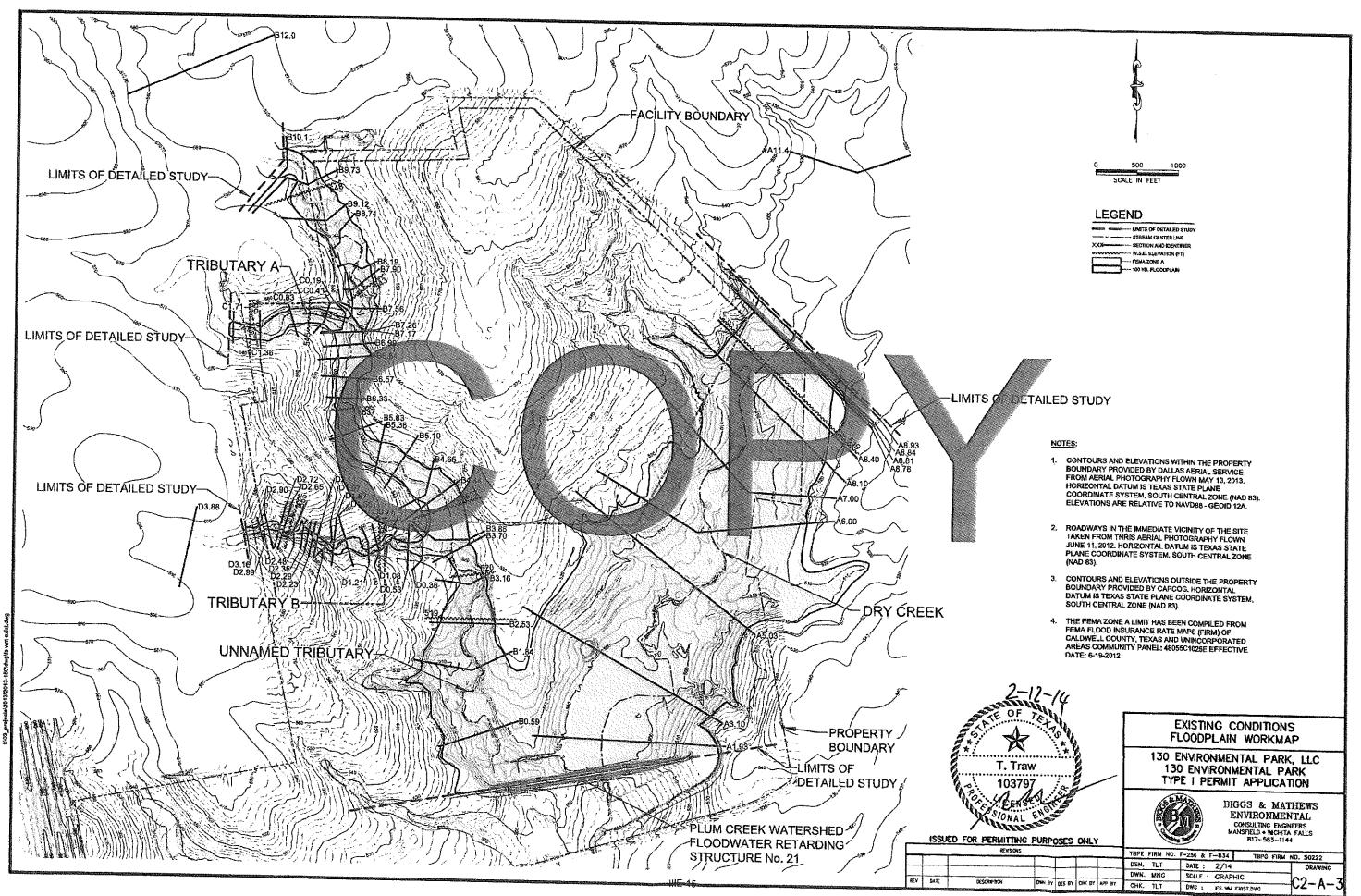
CONTENTS

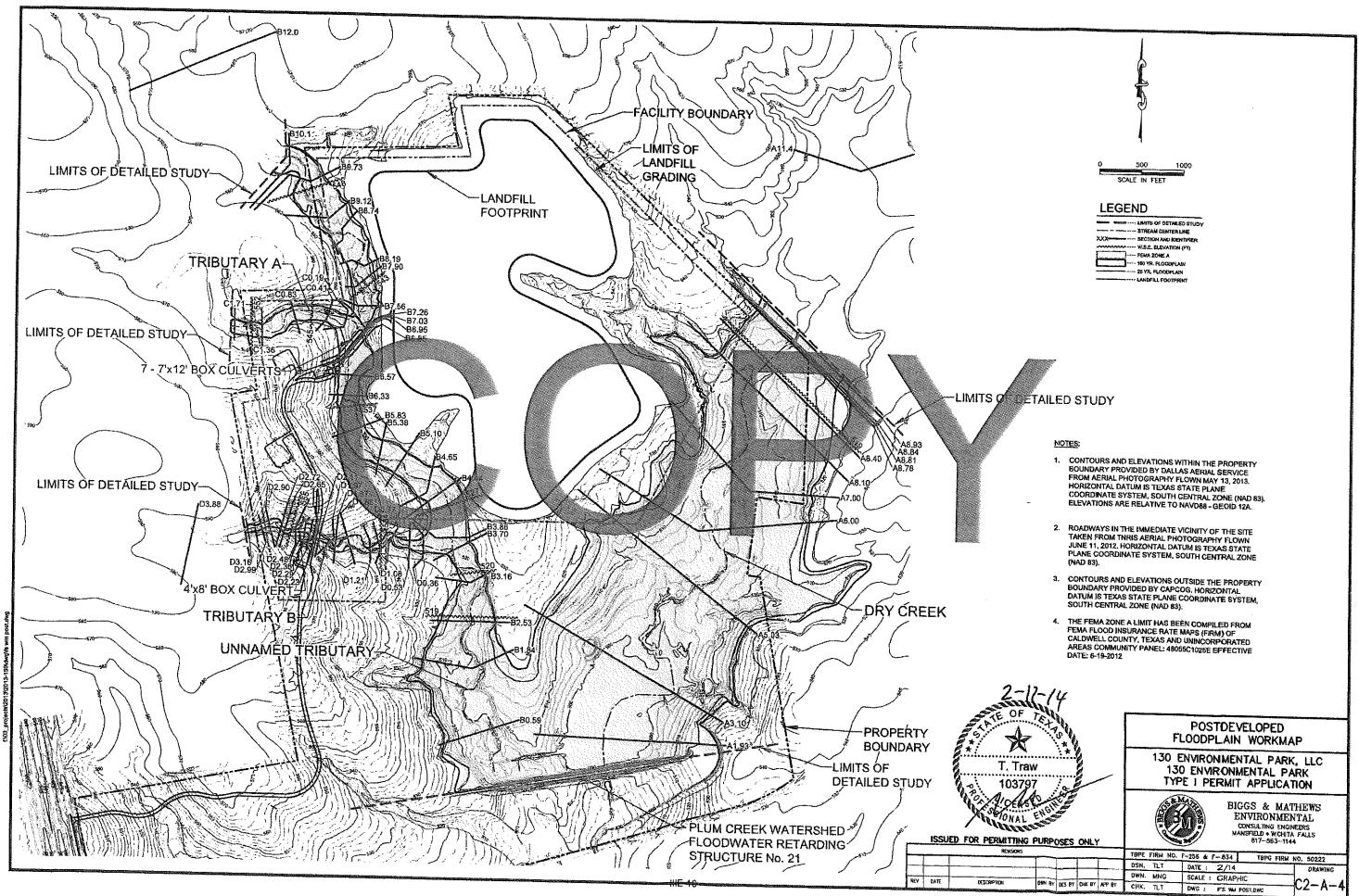
Flood Insurance Rate Map	.C2-A-1
Existing Condition Drainage Areas	.02-4-1
Existing Conditions Floodplain Workmap	.O2-A-2
Post-Developed Floodplain Workmap	
Post-Developed Floodplain Workmap – Detail	.02-A-4

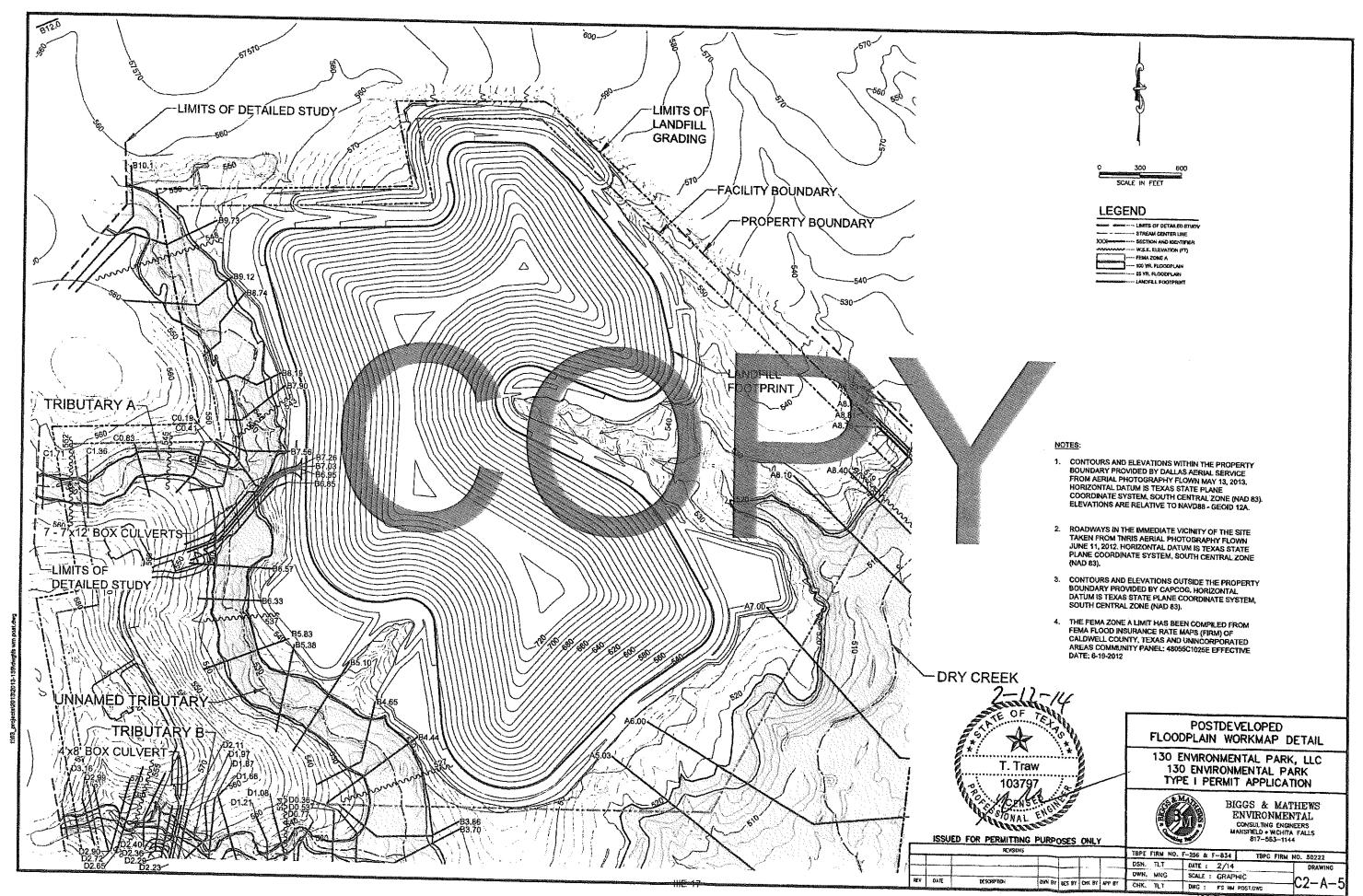












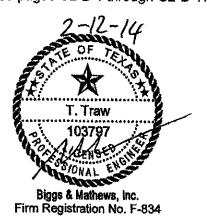
130 ENVIRONMENTAL PARK

ATTACHMENT C2

APPENDIX C2-B

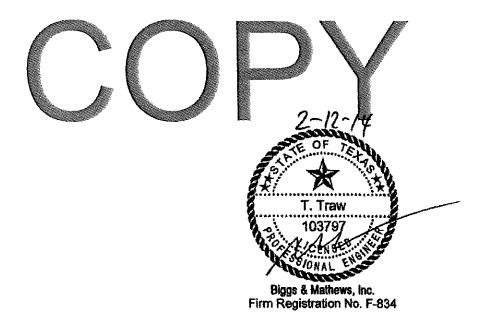
EXISTING CONDITIONS HEC-HMS EVALUATION

Includes pages C2-B-1 through C2-B-17



CONTENTS

Existing Condition Discharge Summary	C2-B-1
Watershed Characteristics	C2-B-3
Rainfall Data	C2-B-6
Site 21 Reservoir Data	C2-B-9
HEC-HMS Schematic	C2-B-11
Hydrologic Analysis	C2-B-13



EXISTING CONDITION DISCHARGE SUMMARY

130 Environmental Park Existing Conditions Discharge Summary

Flow Change Location/Cross-Section	100-Year Peak Discharge (cfs)	25-Year Peak Discharge (cfs)	Hydrologic Element
A11.4	5381.0	3939.6	Basin: DC-2
A7.00	7266.0	5326.5	Junction: Dry Creek
B12.0	1933.4	1410.5	Basin: UNT-5
B7.17	2909.0	2127.1	Junction: North
B3.7	3803.2	2761.0	Junction: South
C1.71	975.7	716.6	Basin: UNT-4
D3.88	337.2	245.4	Basin: UNT-2

WATERSHED CHARACTERISTICS

130 Environmental Park Watershed Runoff Curve Numbers Existing Watershed Characteristics

		<u>-</u>					т		
	Water, CN = 98	28.09	2.66	0.16		4,11	174.59	31.66	
p (ac)	Woods (fair), CN = 79	106.03	44.85	104.89	81.36	17.50	245.70	455.85	
nd Soil Grou	Residential (1 ac), Soil Group D, CN = 84							70.87	
Partial Areas of Cover Type and Soil Group (ac	Paved (w/ROW), Soil Group D, CN = 93		0.32		91.85	11.02	4.00	57.91	
I Areas of C	Pasture (fair) Soil Group 0, CN = 84	40.40	4 78	4.82	/3 :25	3.57	4.67		
Partia	Pasture (good),	95'7			105.08	545.12	31.58	1611.60	
	Brush (fair), Soil Group D, Γζ = NO	15.73	82.05	31.94	166.95	332.63	424,10	677.49	
	CN (Weighted)	82	78	79	8	79	82	8	
	Watershed Area (² .iM)	0.253	0.210	0.222	0.701	1.428	1.382	4.540	
	Matershed Area (26)	161.82	134.66	141.81	448.48	913.94	884.64	2905.38	
	omeN baderateW	INT-1	UNT-2	UNT-3	UNT-4	UNT-S	DC-1	DC-2	

Biggs & Mathews Environmental M:\Proj\f29\06\101\P\Part 3 Att C2 Tables.xlsx Existing Lag Time

130 Environmental Park SCS Unit Hydrograph Lag Time Existing Watershed Characteristics

										
(L	lim) əmiT gs.J	107	25	32	70	70	29	85	. 87	
	Time of Conc. (hr)	2.97	1.57	0.88	707	70	0.80	2.35	2.42	
≩	Time (hr.)	0.96	0.00	000		07'0	0.08	0.14	0.23	
Channel Flow	Water Course Length (ft)	14140	0	c		2840	995	1437	2943	
ີ່ວັ	Avg, Bank Full Velocity (fps)	4.08	0.00	000	100	3.27	3.50	2.86	3.52	
×	Time (hr)	1.62	1.17	0.37	2 .	0.45	0.21	1.34	1.78	
Shallow Conc. Flow	Water Course Slope (fl/ft)	0.01	0.01	N 03	3	0.01	0.03	0.01	0.01	NA CONTRACTOR
nallow C	Roughness Inelicited	16.13	613		2	16.13	16.13	0.0	16.13	
S	Water Course Length (ft)	8945	6467	200	3	288.2	1947	6501	8589	CARROLL STATE
	Time (hr)	0.38	0 40	2 2	5.5	1.17	0.51	0.88	0.40	
>	Water Course Slope (fivft)	0.03	0.01		0.0	0.0	0.04	0.01	0.03	
Sheet Flow	Precipitation 2yr Total (in.)	3 60	3.60	2 6	3.00	3.60	3.60	3.60	3.60	
S	Water Course Length (ft)	240	270	7 2 2	007	280	260	275	250	2
	Manning's Roughness	0.24	7.0	2 3	0.13	0.40	0 13	0.24	0.24	7.5
ЭΙ	msM bedstetsW	1	4 7	- - - -	UNI-1	UNT-2	INT.3	Z L	t NI	?

130 Environmental Park Kinematic Wave Routing Parameters Existing Watershed Characteristics

Reach Name	Water Course Length (ft)	Water Course Slope (ft/ft)	Manning's Roughness	Shape	Bottom Width (ft)	Side Slope (xH:1V)
Dry Creek	1000	0.010	0.045	Trapezoid	30.00	5
Reach-2.0	656	0.010	0.065	Trapezoid	17.00	12
Reach-2.1	3455	0.005	0.065	Trapezoid	15.00	25

RAINFALL DATA

7 day 10 day*
7 day
5 day
3 day
2 day
24 hr.
12 hr.
6 hr.
3 hr.
2 hr.
1 hr.
15 min. 30 min.
Duration

13 Year Naturn Period) 1,90 2.50 3.35 4.33 4.71 5.31 6.00 7.70 9.00 9.60 10.00 10.80 13.40	100 Year Return Period) 2.46 3.13 4.42 5.80 6.38 7.00 8.84 10.40 11.70 13.00 13.20 14.20 16.80	
	1.90		2.46	
	Precipitaion Depth (in.)		Precipitaion Depth (in.)	

2004, Atlas of depth-duration frequency of precipitation annual maxima for Texas: U.S. Geological Survey Scientific Imestigations Report 2004-5041, Precipitaion Depths from: Asquith, W.H., and Rousse Implementation Report 5-1301-01-1) *Precipitation Depths from: Technical Paper No. 49; Two to Jen-Day Precipitation for Return Periods of 2 to 100 Year in the Contiguous United States

C2-B-7

Duration	5 min.	5 min. 15 min. 30 m	30 min.	1 hr.	2 hr.	3 hr.	6 hr.	12 hr.	24 hr.	2 day	4 day	7 day	12 hr. 24 hr. 2 day 4 day 7 day 10 day*

						125 YE	25 Year Return Period	Period					
Precipitaion Depth (in.)	1.69	2.24	2.68	3.20	3.82	4.24	40'5	90'9	7.24	8.65	10.34 11.94	11.94	13.09
	100 Year	100 Year Return Peri	eriod			7				:			
Precipitaion Depth (in.)	2.21	2.94	3.52	4.21	5.04	5.59	6.899	8.00	9.57		11.45 13.70	15.83	17.36

Precipitation depths used in the 10 day frequency storm meteorlogical model within the HEC-HMS hydrological model for flood analysis. Precipitation depths were "smoothed" using regression methods as suggested in the HEC-HMS Technical Reference Manual.



22-8-8

SITE 21 RESERVOIR DATA

130 Environmental Park **Pond Data for HEC-HMS**

Site 21

Reservoir

Description:

Downstream:

CP8

Method:

Outflow Structures

Storage Method:

Elevation-Area-Discharge

Elev-Area Function:

Site 21 Elev Area

Elev-Dis Function Primary: Site 21 Elev-Discharge Elevation-Discharge

Initial Condition:

Elevation

Initial Elevation: 498.5 ft

Paired Data

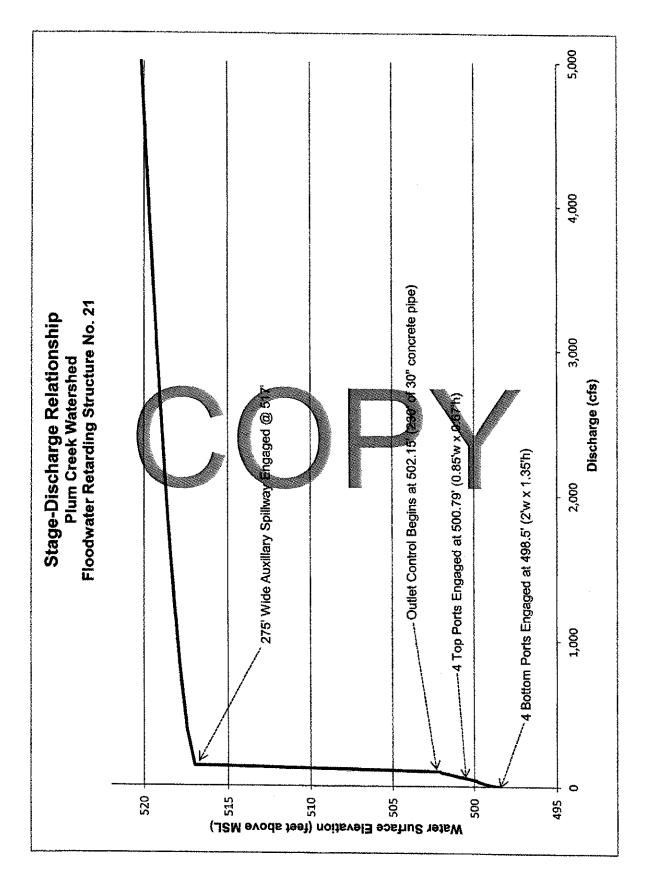
Elevation Storage Functions

Site 21 Elev Area

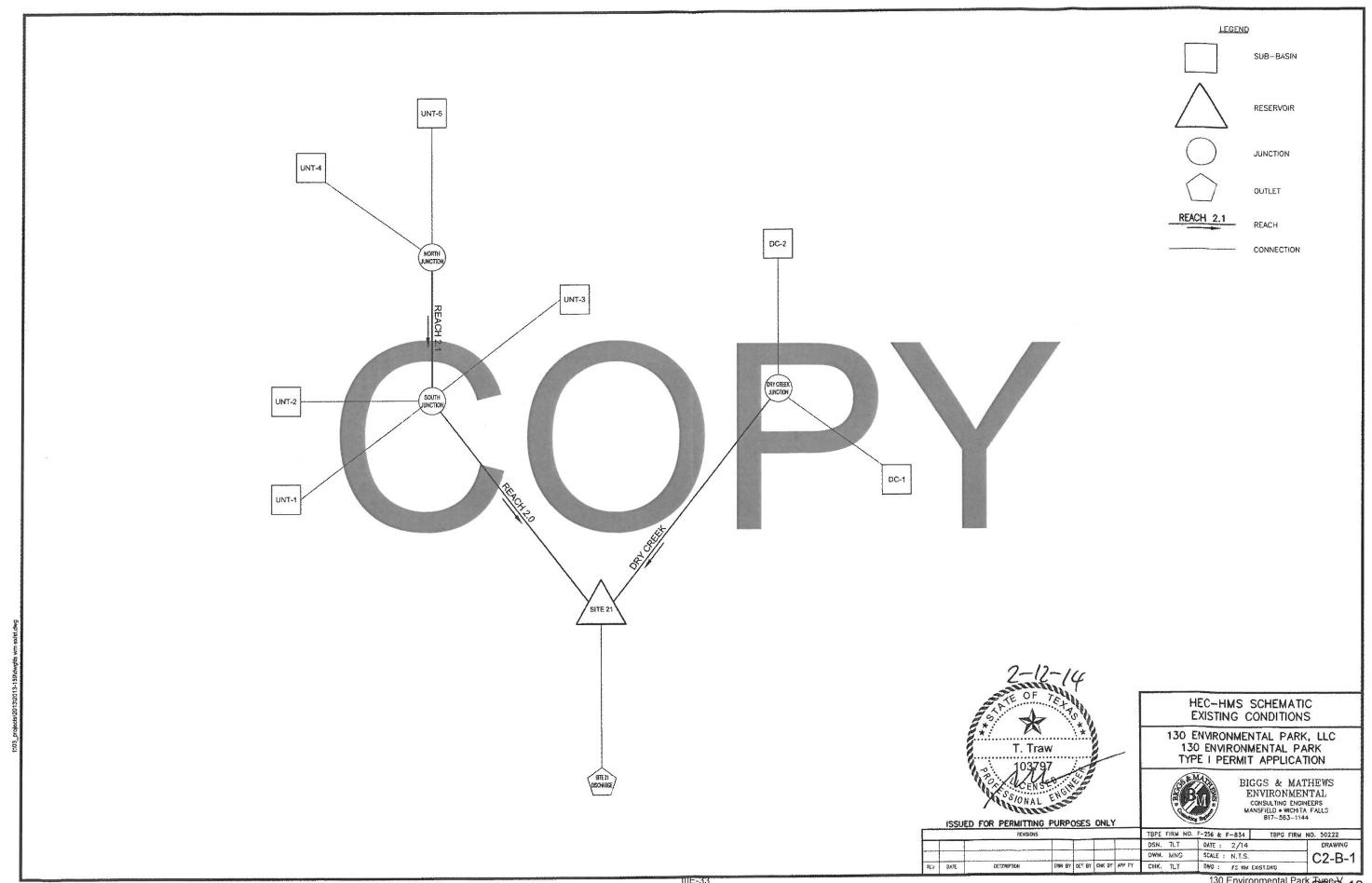
Elevation	Area	Volume
(ft)	(ac-ft)	(ac-ft)
498.10	22.00	0.00
502	54.75	149.66
504	81.00	285.41
506	113.05	479.45
508	141.47	733.97
510	173.17	1048.60
512	204.87	1426.65
514	256.45	1887.97
516	296.24	2440.66
518	343.69	3080.59
520	411.10	3835.38
522	455.40	4701.88

Paired Data Devation Discharge Function Site 21 Elev-Discharge

Elevation	Discharge	Elevation	Discharge	Elevation	Nicobana		p. 1
ł			Discharge		Discharge	Elevation	Discharge
(ft)	(cfs	(50)	(cfs)	(ft)	(cfs)	(ft)	(cfs)
498.50	0.02	50 0.20	48.50	501.90	88.33	516.32	137.50
498.60	0.83	500.30	50.78	502.00	90.35	517.43	382.71
498.70	2.18	500.40	52.97	502.10	92.31	517.87	839,48
498.80	3.91	500.50	55.08	502.15	100.00	518.10	1134.54
498.90	5.94	500.60	57.10	502.96	102.50	518.32	1447.38
499.00	8.25	500.70	59.06	503.78	105.00	518.56	1819.62
499.10	10.79	500.80	60.96	504.62	107.50	518.78	2187.12
499.20	13.54	500.90	63.11	505.49	110.00	519.23	3010.38
499.30	16.50	501.00	65.43	506.37	112.50	519.70	3963.76
499.40	19.65	501.10	67.84	507.28	115.00	520.16	4981.12
499.50	22. 9 8	501.20	70.33	508.20	117.50	520.63	6100.01
499.60	26.48	501.30	72.88	509.16	120.00	520.86	6675.17
499.70	30.13	501.40	75.49	510.12	122.50	521.10	7293.83
499.80	33.95	501.46	77.08	511.10	125.00	521.57	8558.14
499.84	39.16	501.50	79.45	512.10	127.50	522.04	9889.19
499.90	40.87	501.60	81.82	513.13	130.00		
500.00	43.56	501.70	84.07	514.17	132.50		
500.10	46.09	501.80	86.24	515.24	135.00		



HEC-HMS SCHEMATIC



HYDROLOGIC ANALYSIS

Project: 130 Environmental Park Simulation Run: 100yr 10day (smoothed)

01Jan2013, 00:00 Start of Run:

13Jan2013, 00:00

Basin Model:

Existing

End of Run:

Meteorologic Model: 100 yr 10 day (smoothe

Compute Time: 21Jan2014, 17:36:47 Control Specifications: 12 days

Hydrologic Element	Drainage Area (Ml2)	Peak Discharg (CFS)	eTime of Peak	Volume (AC-FT)
DC-1	1.38	2046.3	06Jan2013, 01:30	1095.6
DC-2	4.54	5381.0	06Jan2013, 02:00	3532.9
Dry Creek	5.92	7252.1	06Jan2013, 01:45	4628.9
Dry Creek Junction	5.92	7266.0	06Jan2013, 01:45	4628.4
North Junction	2.13	2909.0	06Jan2013, 01:30	1651.6
Reach-2.0	2.81	3775.4	06Jan2013, 01:30	2179.3
Reach-2.1	2.13	2900.9	06Jan2013, 01:45	1651.0
Site 21	8.73	2346.5	06Jan2013, 05:00	4828.2
Site 21 Discharge	8.73	2346.5	06Jan2013, 05:00	4 828.2
South Junction	2.81	3803.2	06Jan2013 01:30	2179.0
UNT-1	0.25	442.7	06dan2013, 01:00	198.5
UNT-2	0.21	337.2	06Jan2013, 0 5	160.0
UNT-3	0.22	3978	06Jan2013, 0 00	169.4
UNT-4	0.70	975.7	06Jan2013, 01:30	550.2
UNT-5	1.43	1933.4	06Jan2013, 01:30	1101.3

Project:

130 Environmental Park

Simulation Run:

100yr 10day (smoothed)

Site 21

Start of Run:

01Jan2013, 00:00

Basin Model:

Existing

Reservoir:

End of Run:

13Jan2013, 00:00

Meteorologic Model:

100 yr 10 day (smoothed)

Compute Time:

21Jan2014, 17:36:47

Control Specifications:

12 days

Volume Units:

_ ___

AC-FT

Computed Results

Peak Inflow:

11001.7 (CFS)

Date/Time of Peak Inflow:

06Jan2013, 01:45

Peak Outflow:

2346.5 (CFS)

Date/Time of Peak Outflow:

06Jan2013, 05:00

Total Inflow:
Total Outflow:

6808.3 (AC-FT) 4828.2 (AC-FT) Peak Storage : Peak Elevation :

3391.3 (AC-FT) 518.9 (FT)

Project: 130 Environmental Park Simulation Run: 25yr 10day (smoothed)

Start of Run: End of Run:

01Jan2013, 00:00 13Jan2013, 00:00

Basin Model:

Existing

Meteorologic Model: 25 yr 10 day

Compute Time: 24Jan2014, 12:45:08 Control Specifications: 12 days

Hydrologic Element	Drainage Area (MI2)	Peak Discharg (CFS)	eTime of Peak	Volume (AC-FT)
DC-1	1.38	1508.5	06Jan2013, 01:30	788.3
DC-2	4.54	3939.6	06Jan2013, 02:00	2526.7
Dry Creek	5.92	5314.9	06Jan2013, 01:45	3315.5
Dry Creek Junction	5.92	5326.5	06Jan2013, 01:45	3315.1
North Junction	2.13	2127.1	06Jan2013, 01:30	1180.0
Reach-2.0	2.81	2740.0	06Jan2013, 01:45	1557.3
Reach-2.1	2.13	2118.9	06Jan2013, 01:45	1179.7
Site 21	8.73	382.9	06Jan2013, 16:00	3015.5
Site 21 Discharge	8.73	382.9	06Jan2013, 16:00 /	8015.5
South Junction	2.81	27610	06Jan2013, 01:30	1557.0
UNT-1	0.25	326.3	06dan2013, 61:00	142.8
UNT-2	0.21	245.4	06Jan2013, 0 15	113.7
UNT-3	0.22	290,6	06Jan2013, 0 00	120.8
UNT-4	0.70	716.6	06Jan2013, 01:30	394.8
UNT-5	1.43	1410.5	06Jan2013, 01:30	785.2

Project: 130 Environmental Park

Simulation Run: 25yr 10day (smoothed) Reservoir: Site 21

Start of Run:

01Jan2013, 00:00

Basin Model:

End of Run:

13Jan2013, 00:00

Meteorologic Model:

Existing

Compute Time:

24Jan2014, 12:45:08

Control Specifications:

25 yr 10 day 12 days

Volume Units:

AC-FT

Computed Results

Peak Inflow:

8054.8 (CFS)

Date/Time of Peak Inflow: Date/Time of Peak Outflow: 06Jan2013, 01:45

Peak Outflow: Total Inflow:

382.9 (CFS) 4872.8 (AC-FT)

Peak Storage:

06Jan2013, 16:00 2888.1 (AC-FT)

Total Outflow:

3015.5 (AC-FT)

Peak Elevation:

517.4 (FT)

130 ENVIRONMENTAL PARK ATTACHMENT C2 APPENDIX C2-C

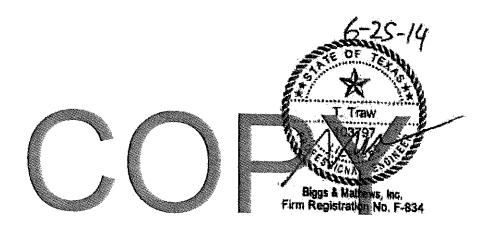
EXISTING CONDITIONS HEC-RAS EVALUATION

includes pages C2-C-1 through C2-C-77

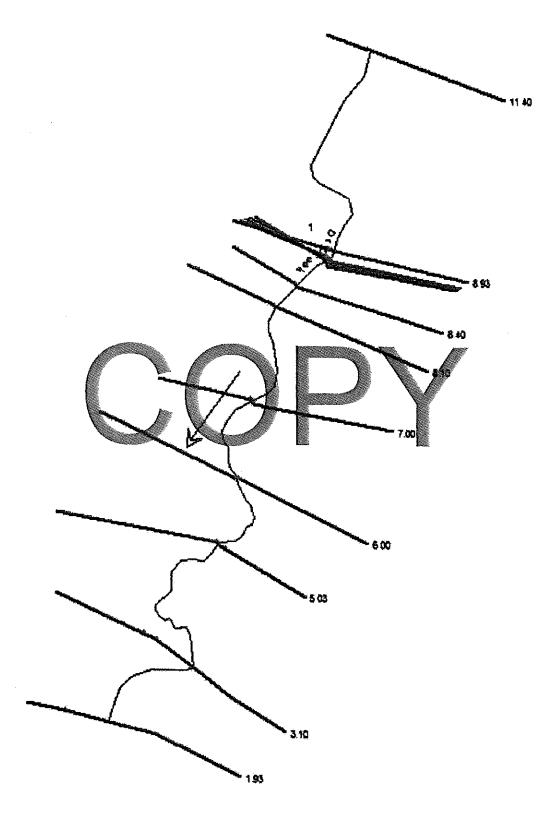
Biggs & Mathews, Inc. Firm Registration No. F-834

CONTENTS

Existing Condition HEC-RAS	Schematic	.C2-C-1
Existing Condition HEC-RAS	Analysis	.C2-C-4



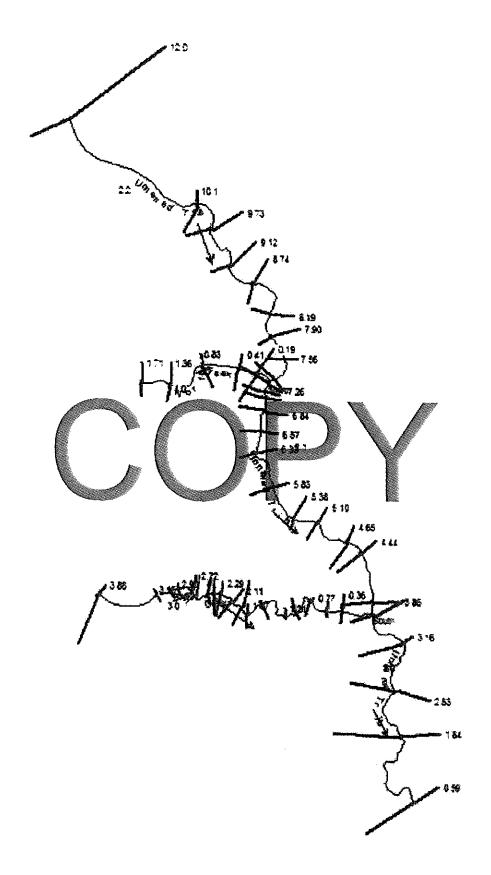
EXISTING CONDITION HEC-RAS SCHEMATIC



Biggs & Mathews Environmental
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C2-C-2

130 Environmental Park - Type I
Rev. 0, 2/12/2014
Part III, Attachment C2, Appendix C2-C
130 Environmental Park Type V
Part III, Appendix IIIE



Biggs & Mathews Environmental
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C2-C-3

130 Environmental Park – Type I Rev. 0, 2/12/2014 Part III, Attachment C2, Appendix C2-C 130 Environmental Park Type V Part III, Appendix IIIE

EXISTING CONDITION HEC-RAS ANALYSIS

11 140 11 140 11 183 11 184 11 184	25/r 25/r 25/r 25/r	(dfs) 5381.00 3939.60		(ft) 521.38	(ff) 521.38	(h)	Este Signe (m)	Ver Unit	(sq.ft)	(ii)	Frouder#Cfil
0		5381.00 3939.60	514.60	521.38	(ff) 521,38	(m)	(MM)	(u/s)	(8q.ft)) (u)	
ei o	25/c (25/c (25/c (25/c (25/c (25/c (25/c	5381.00 3939.60	514.60	521.38	521,38	2000	The second secon				
	100 yr. 100 yr. 100 yr.	3939.60				\$77.04	0.035746	8.80	1152.96	746.25	0.74
	(00 yr (00 yr (5) yr		514,80	521.12	521.12	521.67	0.030491	7.80	957.88	725 27	0.87
	100 yr 100 yr 151 yr										
	5.77 (00)7 (5.77	5381.00	506.00	519.14	513.23	519.15	0.000099	1.16	6021.98	1361.27	900
	15.77 15.77	3939.60	506.00	517.64	er su	517.86	0.000147	1.29	4130,43	1171.05	70.0
	557 557 00 yr										
	5.7°	5381.00	506.00	519,13	514.07	\$19.14	0.000127	1,19	5885.99	1323.34	0.07
	00 rt.	3939.60	506.00	517.6	513.53	\$17.64	0.000178	1.27	4094.37	1088.03	0.08
が対象が行る。例が、「はない」というできょう。これできる。	00 yr.										
8.81	\$ 00 kg	Culvert									
	00 yr										
87.8	a de	5381.00	505.89	519.07		519.09	0.000217	1.68	5951.36	1321.31	0.09
8.78	Z-7/C	3939.60	505.89	517.61		517.63	0.000278	1.70	4190.24	1101.00	0.10
	locy.	5381.00	505.09	519.D d		10.01	0.000194	1.65	6714.24	1606.63	0,08
8.40	25 VE	3939.60	505.09	517.50		17.52	0.000283	1,82	4497.96	1346.86	0.10
8.10	100 %	5381.00	504.56	518.98		518.97	0.000090	1.17	9146.12	1799.46	90'0
8.10	25 yr.	3939.60	504.56	517.46		517.47	0.000114	1.21	6638,62	1581,55	0.06
				The second second	Acces (Re-producing producing participation of the control of the	E Sphynger advance		-9,7-			
	¥ 60	7266.00	502.00	518.92		\$18.92	0.000028	0.73	14288.76	1609.42	0.03
7.00	25 yr	5326.50	502.00	517.42		\$17.42	0.000025	0.65	11952,51	1499.68	0.03
	200 yr		502.00	518.91		A\$18.91	0.000012	0.72	20236.27	2123.98	0.03
6:00 2:	25vr	5326,50	502.00	517.41		517.41	0.000009	0.60	17241.55	1843,82	0.03
		,									
8.03	100 %	7266.00	500.00	518.90		\$18.91	0.000007	0.49	23576.79	2115.32	0.02
1508	25 m	5326.50	500.00	517.40		517.40	0.000006	0.41	20489.25	1987.57	0,02
	100.97	7266.00	498.12	518.90		518.90	0.000001	0.28	32791.92	2343.33	0,01
300	25 yr	5326.50	498.12	517.40		517.40	0.000001	0.23	29346.24	2239.22	0.01
	100 yr	7266.00	497.59	518.90	499.05	518.90	0.000001	0.27	32373.33	2207.92	0,01
11,93	25 yr	5326.50	497.59	517.40	498.83	517.40	0.000001	0.22	29172.10	1995.17	0.01

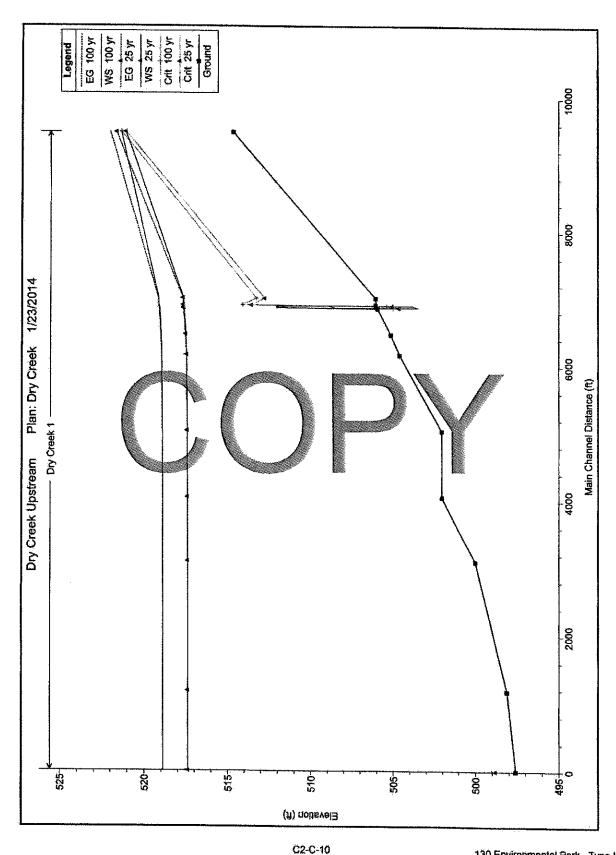
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River	Reach	River Sta	Profile	Q Total	MINCHE	W.S. Elev	CHI W.S	EIG Elev	E.G. Slope	VeliChri	FlowArea	Top Width	Froude # CH
				(cts)	(t)	(tt)) W	(u)	((A)	(£A)	(Sd.ft)	(4)	1
Unramed Trib	2.2	120	100.91	1933,40	555.00	559,03	558.97	560.08	0.017247	1			ge C
Unhamed Trib	22	12.0	25.yr	1410,50	555.00	558.52	558.47	559.43	0.017541				
Unnamed Trib	2.2	10.1	100 yr	1933.40	548.00	550.74		550.93	0.002164	4.06	724.38	403.54	0.35
Unnamed Tith	22	10.1	<u>25</u> yr	1410.50	546.00	550.30		550,47	0.002101	3.73	553.98		
							/						200
Upnamed Tilb	2.2	9.73	100 yr	1933,40	544.26	548.64		549.05	0.013985	6.38	515.06		0.59
Uninamed Trib	2.2		25 yr	1410.50	544.26	548.18	547.75	548.59	0.015071		383,87	27434	
Unhamed Trib	2/2		100 yr	1933.40	539.18	\$46.15		546.26	0.002355	3.47	1014.55	539.36	0.2
Unnamed Trib	2:2		25 yr	1410.50	539.18	545708		545,79	0.002290	3.23	773,58		0.25
					-	Man	2						
Unnamed Titb	2/2		100 yr	1933.40	538.94	545.00	1	545.18	0.003943	4,02	864,84	439.63	0.32
Unnamed Trib	<u>2.2</u>	8.74	25 yr	1410.50	538.94	£44.45	1	544.59	0.004989	4.13	617.91	381.95	0.38
Unnamed Trib	2.2		100 yr	1933.40	536.67	543.85	i.	543.95	0.001608	3.19	941.12	365.22	0.22
Unnamed Trib	2,2	8,19	25yr	1410.50	536.67	543,20		543.28	0.001534	2.90	722.52	303.07	0.21
							Ĭ						
500	252		*85. *	1933.40	535.72	1 2 3	\	543.34	0.003135	4.25	771.96	314.25	0.29
Unnamed Trib	22	7,90	25.yr	1410.50	535.72	542.57		542.69	0,003137	3,96	587.77	257.91	0.29
			100 yr	1933,40	535.18	10.75	240.34	542.14	0.004436	5.21	684.42	294.55	96.0
Unnamed Trib	2.2	7.56	25 yr	1410.50	535,18	541.24		541.42	0.004936	20.5	492.29	228,93	0.37
	2.2		100 yr	1933.40	533,95	540.99		541.15	0.002947	4.20	744.29	252,23	0.30
Unnamed Trib		7.26	25.yr	14.10.50	533.95	540.15)	540.31	0.003254	4.01	549.23	211.36	0.30
	2:1		100 yr	2909.00	534,38	540.57	Ň	540.81	0.004334	4.87	898.42	300,89	96.0
Unnamed This	251	7.17	25 yr	2118.90	534.38	539,73		539,95	0.004509	4.48	673.28	242.25	56.0
	ম		700 yr	2909.00	533.20	100		540.40	0.003616	4.61	809.58	228.77	0.33
Unnamed Tife			25 yr	2118.90	533.20	539.32		539.54	0.003492	4.12	638.29	194.58	0.31
			-										
8	7.1		JA On L	2909,00	531.88	539.90		540.17	0.003521	4.92	812.67	244.53	0.33
Unnamed Trifb		6.99	25yr	2118.90	531.88	539:08		539.31	0.003367	4.42	631,71	200.48	0.31
Unnamed Trib	1.2	5.84	300tyr	2909.00	531.63	539.66		539.76	0.001525	3.52	1566.13	446 12	22.0
		6,84	25 yr	2118.90	531.63	538.80		538.90	0.001638	80	F0.K0+1	474 77	n 24
		4.57	.¥.001	2909.00	530.49	538.99		539.21	0.002806	4.31	975.43	269.30	0.28
A Property	The Control of the Co	Control of the second	The second secon										

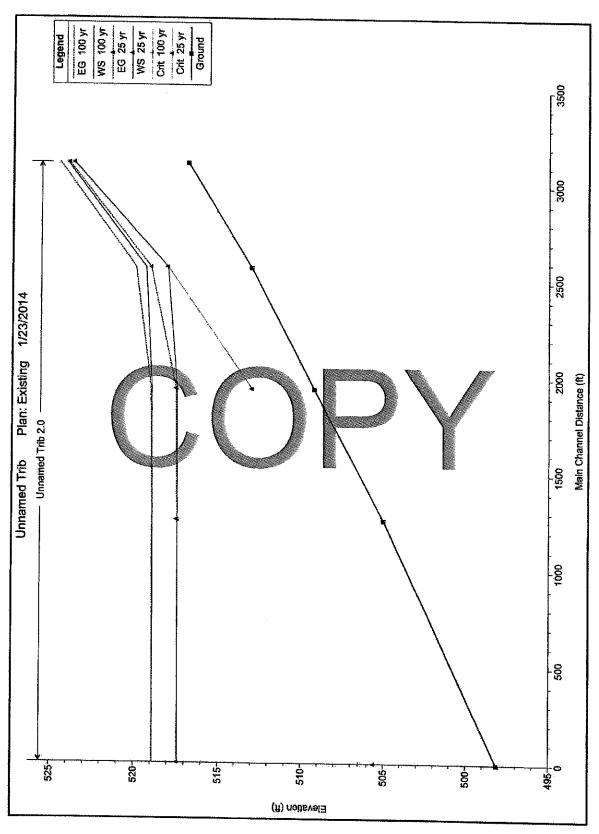
KIVET	Keach	KNersta	Profile	O Total	Minchel	W.S. Elev	Crtt W.S.	E.G. Elev	E.G. Slope	Vel Chri	FlowArea	Top Width	Froude # Chi
				(68)	T w	(u)	<u>m</u>	(m)	(¥/¥)	(s/u)	(sq fi)	(£)	
							-						
Unnamed Trib	23.1	6,33	100 yr	2909:00	530.55	537.97		538.31	0.005338	28'9	810.94	256.11	0,40
Unnamed Trib	5:1	6.33	25 yr	2118.90	530,55	537.22		537.52	0.005142	5.32	630.40	223.29	0.38
Unramed Trib	2.1	5:83	100 yr	2909.00	527.28	535,23		532.55	0.006706	6.51	778.38	255.77	4.0
Unnamed 11b	23	583	[25 yr	2118.90	527.28	13.19		534.80	0.006852	603	606.39	225.92	0.43
Unnamed Trib	2.1	538	100yr	2909.00	525.29	532.81		533.07	0,004352	5.28	928.24	296.77	6.0
Unramed Trib	2.1	5:38	26 yr	2118.90	525.29	532.11		532.35	0.004286	4.87	727.49	281.24	0.35
								tar					
named Trib	2.1	5:10	10031	2909.00	523.57	5.01 Mg		531.77	0,004970	5.40	898.23	300,25	0.38
Unnamed Trib	127	5,10	25.yr	2118.90	523.57	530.91		531.14	0.004435	4.78	728.12	277.14	0.35
						1	1						
Unnamed Trib	12.1	4.65	100 yr	2909:00	521.27	528.95		529.27	0.006901	6.62	945.43	431.63	0.45
Unnamed Trib	2.1	4,65	25 yr	2118.90	521.27	528.43		528.75	0.007022	6.32	722.03	408.82	0.45
lamed Trib	2.1		100 yr	2909.00	520.53	527.62		527.83	0.006230	5.87	1017.00	414.56	0.42
Uninamed Trib	233	2	25 yř	2118.90	520.53	\$27.10		527.30	0.006096	5,47	807.07	389.06	0.41
						1		-					
Unnamed Trib	23.1	3.86	100 yr	2909.00	518.57	525.13		525.27	0.003320	4.06	1264.89	519.55	0.31
Unnamed Trib	ŭ		25 yr	2118.90	518.57	524,48		524.62	0.003657	3,91	942.35	463.22	0.32
A													
Uninamed Tub	0,2	3770	100 yr	3775.40	516.79	524.06		524.51	0.006314	8.16	948,69	319.19	0.43
Unnamed Tirb	20	3.70	25.yr	2740.00	516.79	523.66		523.96	0.004487	4.97	825.96	290.58	0.36
	2.0	3:16	100 yr	3775,40	512.97	519,32)	519,92	0.012554	7.26	775.41	311.24	95.0
Unnamed Trib		3.16	25 yr	2740.00	512.97	518.02	518.02	519:03	0.027811	8.78	421.32	234.95	0.82
Unnamed Trib	2.0	2,53	400yr	3775.40	509.18	518,96	V	519.00	0,000445	1.99	2838.78	644.04	0.12
			25 yr	2740.00	509.18	517.45	612.98	517,50	0.000625	2.06	1919.93	557.07	\$1.0
333													
Unnamed Trib	2,0	1.84	100 yr	3775.40	504.96	518.92		518.93	0.000043	0.80	6750.90	1032.00	0.04
Umamed Trib		7,84	25yr	2740.00	504.96	517.42	1	517.42	0.000043	0.73	5320.17	867.01	900
			100 yr	3775.40	498.13	518,90	508,54	518.90	810000.0	0.65	9569.92	938.57	9.03
UnnamedTrib	2,0	0.59	žšyr	2740.00	498.13	517.40	505.58	517.40	0.000015	0.56	8288.81	903.26	0.02
1													
	370	3,88	100 yr	337.20	580.00	581,50	580.97	581.60	0.009409	2.91	147.05	151.83	0.42
South Creek			25 yr	245.40	580,00	581,30	580.82	581.38	0.009012	2.59	118.20	137.49	0.40
		1											
South Circex	3	0.10	TROYE	337.20	267.00	568.68	_	569.01	0.041998	6.61	84.58	76.00	06.0

Diam.	Reach	RiverSta	Profile		Min.Ch.El	W.S. Eley	CAT W.S.	E.G. ERV	E.G. Slope	Vel Chri	Elow Area	Top Width	Effected # Cki
				(cts)	(#)	(#)	(u)	w	(A)	(#/e)	(Fee to		H BOOK !
South Creek 3	06	3.16	25 yr	245.40	567.00	568.43		-	D Odese7		3		
									room are		03,24	72.50	0.92
South Creek 3	970	2,39	W.Q0.	337.20	563.05	FRE AT		40 000	100000				
			25 ur	24× 80	20.000			40°CaC	10/11/00	3.80			0.48
Ī				243.40	co.coc			565.30	0.011388	3.35	80.63	63.56	0.47
Court Crook	1	200	400	i i	7 7 7								
I	l		I ACOM	337.70	T8.190		6	Ì	0.021087	4.87	89.08	75.85	0.64
SOUTH CLEBEK	3	08.2	25 V	245.40	561.91	\$63.55	263 S	563.80	0.021287	4.38	69.66	67.84	0.63
	000		100 yr	337.20	554.76	557.72	557.7	558.56	0.053903	7.33	46.01	27.62	4 60
South Creek 3		27.2	25 yr	245.40	554.76	557.32	2299	558.06	0.057514	169	35.50	24.45	*0.*
							1					OLUL Y	2
			100 yr	337.20	554.11	556,58	555.84	556.70	AZCOLU O	2 89	4/10 CT	84 00	3
South Creek 3	3.0		25.vr	245.40	554.41	558.24	644 58	856 30	201000	20.00	102.37	0/.00	0.46
						\		200,000	0.71 2.0	10:0	06.07	LETPO	0.47
South Creek 19		7.48	400	AC-75E	25 033	. cco m		7 7 6 6	-				
THE CHANGE			1000	UA: 160	300.36	003.7U		554.17	0.022857	5.50	62.16	32,46	0.67
Count MI WAR		2 0 0 0	7/.02	245.40	550.38	553.39		553.74	0.020694	4.70	52.37	30.68	0.62
									,				
South Creek 3.0		2:38	100 yr	337.20	549.54	\$51.79	1	552,13	0.024346	5,22	85.03	78.41	ń ea
South Creek 3.(25 yr	245.40	549.54	9	\	551.82	0.024728	4.72	8.5 K.2	60 00	20.0
							+				20.00	60.00	do'n
South Greek 3.0		2.29	100 tr	337.20	547.28	549.93	549 64	550 38	apocen n	20.8	70 04	10 20	***
South Creek 13.0			3cm	SAKAD	547.00			65.1	20000000	0.00	0.00	00'70	0.70
		l		2	A11.40	30 B 40	No. of the last of	25.940	0.022131	5.32	59.40	49.97	79.0
South Crash			1	207.00	441			(
200		1.50	1,000	02.700	044,08	546.93		547.21	0.015195	4.55	88.86	59,80	0.56
Soull break			o yr	245.40	544.58	546.61		546.84	0.015274	4.08	70.49	55.72	0.54
I													
			100 M	337.20	542,05	544.91		545.20	0.013285	4.67	92.31	62.12	0.53
South Creek 13.0		4.97	5.yr	245,40	542.05	544,54	۲	544.79	0.013833	4.28	69.02	54.42	0.53
							V		-				
			700 yr	337.20	541.35	543.84		544,04	0.008963	3.69	97.68	52.87	0.43
South Creek 3.0		1.07	25 yr	245.40	541.35	16 025		543.69	0.007834	3,13	82.33	50.23	0.40
							1						Š
			100.yr	337.20	539.78	541.98	/	542.13	0.009260	3.45	128.21	108 dR	A.43
South Creek 3.0	1,66		Żć.yr	245.40	539.78	541.63	7	541,78	0.010786	3,27	91.86	90.12	0.45
				The state of the s									
South Creek 30			100 yr	337.20	532.89	535,40	535:00	535.88	0.026395	6.46	76.22	60.92	0.75
South Preek 3.0	1.2		25 yr	245.40	532.89	535.13	<u> </u>	535.46	0.021140	5.32	61.78	45.79	D AR
													S
South Greek 3.0	1108		100 X	337.20	531.07	534.07		534.21	0.006541	3.17	127.35	83.73	0.37
South Greek 3:0			1	JAK AM	10 407	17							10.5
				740,45	20.00	533.63		533.76	0.007015	70.00	20.00	200	***

River Reach R	Reach	RiverSta	Profile	a Tótal	MIN.Ch.El	W.S. Elev	CHWS	E.G. Elev	ErG. Slone	VarCsnl	Elne bras	The Walter	Charles & Abs
				(cfs)	w)	Œ	€	₩.	(A)A)	(Are)	(9 kg)	inos dos	
South Creek	3.0	7.10	180 vr	337.20	527.80	532 34			D DOCKSON	Jean -	8	L)	
South Creek	3.0	7/20	25.yr	245.40	527.80	531.92			0.004171	2.74	26.92	92.79	
									· Crano	140	10.00		Lero
South Creek	3.0	0.53	100,54	337.20	528,00	529.45	529.45	529.87	0.050737	5.85	75 03	04 80	200
South Creek	3.0	6,53	25 yr	245,40	528.00	529.27			0.051032	5.28	58 38	85.03	
South Creek	3.0	98'0	100 yr	337.20	523.75	626.25	524.84	526.29	0.000755	1.62	304.77	206.14	0.18
South Creek	3.0	98.0	25 yr	245.40	523.75	525.46	524.67	525.52	0.002102	2.08	159,84	155.10	
North Creek	4.0	1771	1100 yr	975.70	552.00	\$53.90			0.035119	6.57	223.42	186.46	0.84
North Cheek	4.0	1771	25 yr	716.60	552.00	8 8 18	553.48	554,00	0.051292	6.74	152.31	156.89	-
North Craek	4,0	1,36	100 yr	975.70	546.00	250.30		250.90	0.004631	4.23	360,83	152.39	0.35
North Oteak	4.0	1,36	25 yr	716,60	546.00	S. D. 25	548 65	550,40	0.003985	3.66	295.64	136.88	0.32
North Creek	4.0	0,83	100 yr	975.70	544.00	547.08		547.33	0.011148	4.85	309.59	185.15	0.51
North Craek	4.0		25.yr	716.60	544,00	546,55		546.82	0.014462	4.82	218.78	159.96	0,56
	4.0		180'yr	975.70	539.61			543.36	0.008447	4.48	306.54	173.87	0.45
North Greek	4.0	0.44	25 yr	718.60	539.51	542.90		543.07	0.006196	3.66	270.42	185.37	0.38
North Creek	4.0	9,49	100 yr	975.70	538.00	541.67		541.75	0.006128	3.99	400.20	255.47	0.39
	0 .		25yr	716.60	538.00	540.82		541,09	0.014078	5:02	222.51	11.961	0.56
							200						



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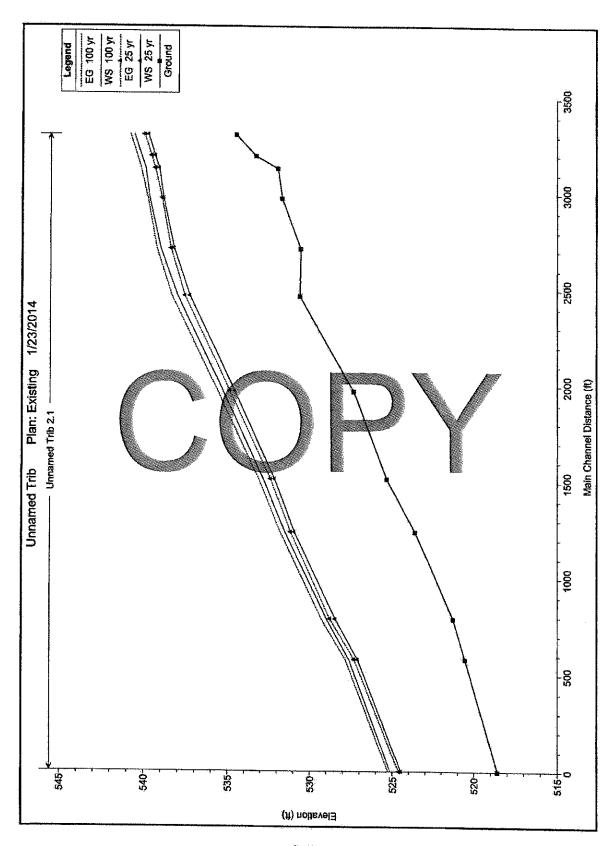
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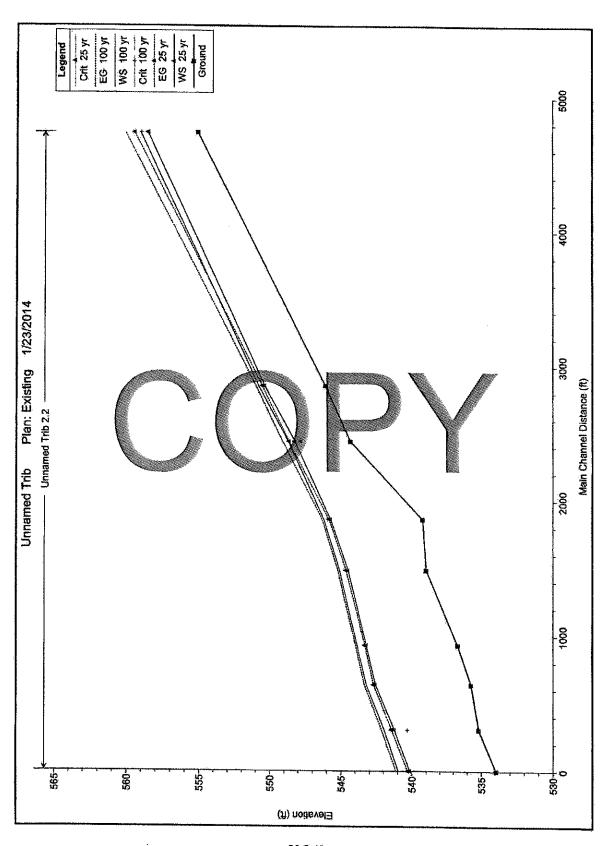
130 Environmental Park - Type I Rev. 0, 2/12/2014 Part III, Attachment C2, Appendix C2-C

130 Environmental Park Type V Part III, Appendix IIIE



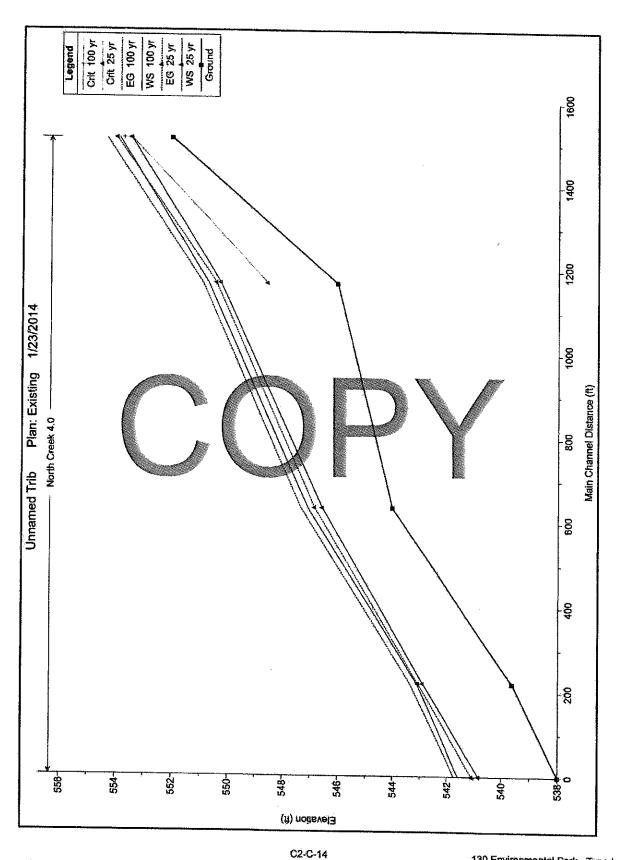
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130 Environmental Park - Type I Rev. 0, 2/12/2014 Part III, Attachment C2, Appendix C2-C 130 Environmental Park Type V Part III, Appendix IIIE



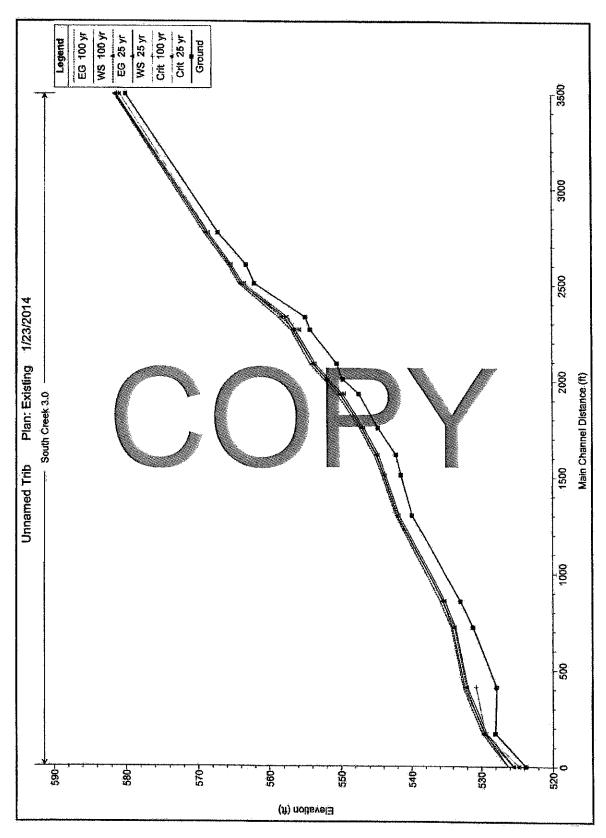
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130 Environmental Park - Type I Rev. 0, 2/12/2014 Part III, Attachment C2, Appendix C2-C 130 Environmental Park Type V Part III, Appendix IIIE

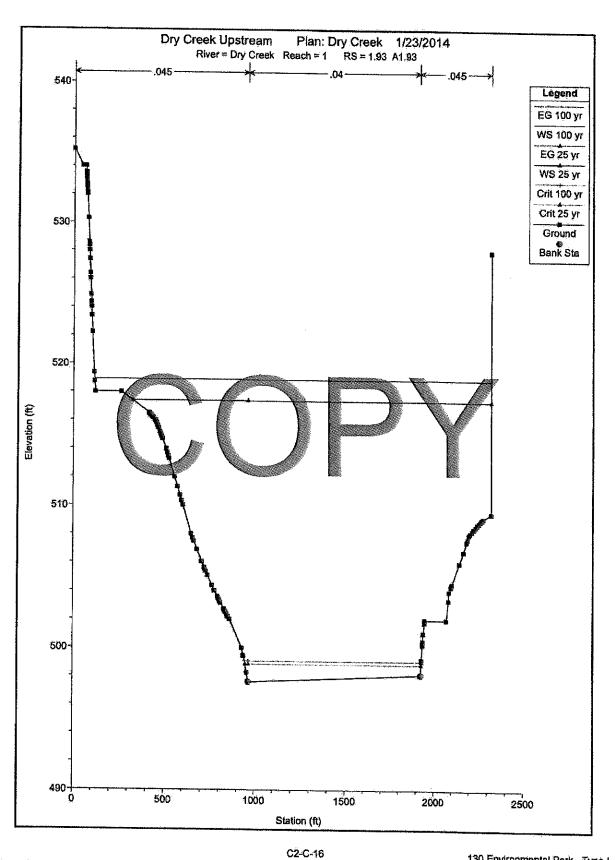


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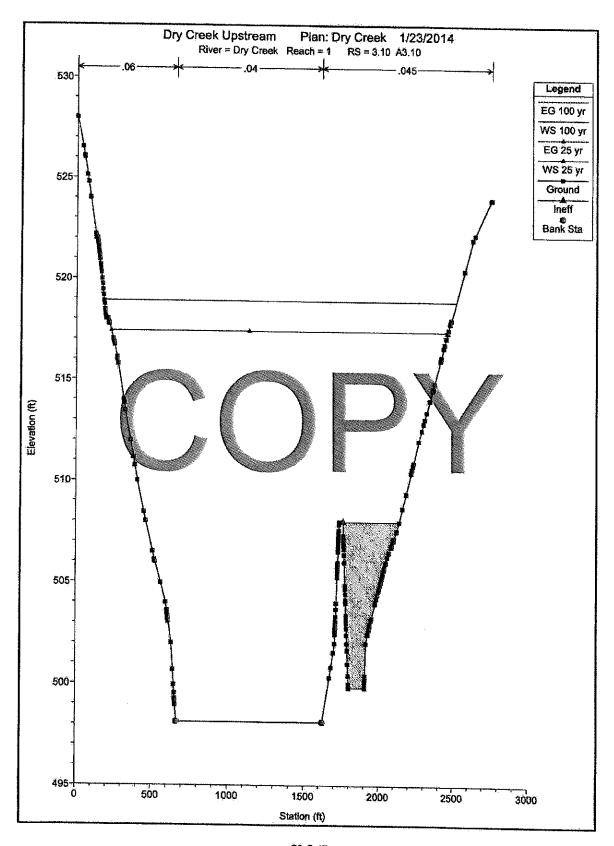
130 Environmental Park - Type I Rev. 0, 2/12/2014 Part III, Attachment C2, Appendix C2-C 130 Environmental Park Type V Part III, Appendix IIIE



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IIIE-56



C2-C-17
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